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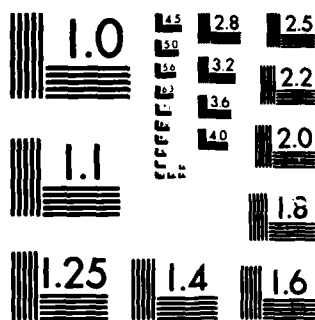
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E. Isaacson, D. Marchesin,
B. Plohr and B. Temple

Mathematics Research Center
University of Wisconsin—Madison
610 Walnut Street
Madison, Wisconsin 53705

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THE CLASSIFICATION OF SOLUTIONS OF QUADRATIC RIEMANN PROBLEMS (I)*

E. Isaacson**^{4,5,9,10,11}, D. Marchesin***^{3,4,5}, B. Plohr^{4,5,7,8}
and B. Temple^{1,2,6,7,8}

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ABSTRACT

We are interested in classifying the solutions of Riemann problems for the 2×2 conservation laws which have homogeneous quadratic flux functions. Such flux functions approximate an arbitrary 2×2 system in a neighborhood of an isolated point where strict hyperbolicity fails. This problem was motivated by Marchesin and Paes-Leme who discovered such a singularity in a system of equations arising in oil reservoir simulation, [15,17]. In [18], Schaeffer, Shearer, Marchesin and Paes-Leme solved the Riemann problem for this system in a neighborhood of the singular point. In [8], Isaacson and Temple outlined a program for classifying such singularities by means of locating normal forms for the equivalence classes of equations generated by linear changes in dependent variables. A 2-parameter family of such normal forms was found by Plohr. In the important work of Schaeffer and Shearer [17], a new normal form was found which reduced the classification of integral curves to a theorem of Darboux on the classification of umbilic

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**Department of Mathematics, University of Wyoming, Laramie, Wyoming.

***Department of Mathematics, PUC/RJ, 22453 Rio de Janeiro, Brazil.

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points for homogeneous cubic equations, [3]. The integral curves fall into four isomorphism classes, called Regions I-IV. In this paper we give the solution of the Riemann problem for the systems in Region IV which exhibit up-down symmetry. A presentation of the solutions of the corresponding systems in Regions II and III will follow.

Our analysis uses a numerical determination of the Hugoniot loci. Moreover, a new phenomenon occurs in Regions II-IV that does not occur in Region I: lines exist on which one of the eigenvalues has the value of the eigenvalue at the singular point. Bifurcations occur at these lines, and the dynamics of the lines as the parameters in the normal form are varied gives a geometric interpretation of the boundaries between Regions I-III. The program for classifying hyperbolic singular points in 2×2 systems of conservation laws is being carried out jointly by the authors named above.

AMS (MOS) Subject Classifications: 65M10, 76N99, 35L65, 35L67

Key Words: Riemann problem, non-strictly hyperbolic conservation laws, umbilic points

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SIGNIFICANCE AND EXPLANATION

A 2×2 system of conservation laws is a system of partial differential equations of the form

$$(1) \quad \underline{u}_t + \underline{f}(\underline{u})_x = 0$$

where $\underline{u} = (u, v)$, $\underline{f} = (f, g)$ are in $\mathbb{R} \times \mathbb{R}$ and where $x \in \mathbb{R}$, $t > 0$. Such equations arise in gas dynamics, elasticity, oil reservoir simulation and other areas of engineering when diffusion is neglected. In solutions of (1), information travels at speeds λ_1 and λ_2 given by the eigenvalues of the matrix $\frac{\partial \underline{f}}{\partial \underline{u}}$. Since this matrix depends on u, v , the speeds λ_1 and λ_2 depend on the solution, and this leads to the formation of discontinuities called shock waves. The present paper deals with the classification of Riemann problem solutions (solutions which evolve from a single discontinuity at time $t = 0$) near an isolated point at which $\frac{\partial \underline{f}}{\partial \underline{u}}$ is a multiple of the identity, so that $\lambda_1 = \lambda_2$. Such a singularity has no analogue in the linear theory.

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THE CLASSIFICATION OF SOLUTIONS OF QUADRATIC RIEMANN PROBLEMS (I)*

E. Isaacson**^{4,5,9,10,11}, D. Marchesin***^{3,4,5}, B. Plohr^{4,5,7,8} and B. Temple^{1,2,6,7,8}

§1. Introduction

We consider the general 2×2 system of conservation laws with quadratic flux functions

$$(1) \quad \begin{aligned} u_t + \frac{1}{2} \{a_1 u^2 + 2b_1 uv + c_1 v^2\}_x &= 0, \\ v_t + \frac{1}{2} \{a_2 u^2 + 2b_2 uv + c_2 v^2\}_x &= 0. \end{aligned}$$

In particular, we solve the Riemann problem globally for a specific range of the coefficients a_i, b_i, c_i .

System (1) is of interest because solutions of (1) approximate solutions of an arbitrary 2×2 system of conservation laws

$$(2) \quad \tilde{u}_t + \tilde{f}(\tilde{u})_x = 0,$$

where $\tilde{u} = (u, v)$, $\tilde{f} = (f, g)$, in a neighborhood of an isolated hyperbolic singularity.

Such a singularity is an isolated point in a neighborhood of which (2) is hyperbolic and at which the Jacobian

$$A(\tilde{u}) \equiv \frac{\partial \tilde{f}}{\partial \tilde{u}} = \begin{bmatrix} f_u & f_v \\ g_u & g_v \end{bmatrix}$$

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has equal eigenvalues and is diagonalizable. In fact, system (1) is obtained from system (2) as follows. Let $\lambda_1(u) < \lambda_2(u)$ denote the eigenvalues of $\Lambda(u)$, and let u_0 denote the isolated point at which $\lambda_1(u_0) = \lambda_2(u_0) \equiv \lambda_0$. First, replace u by $u - u_0$ and translate the reference frame (x, t) to $(x - \lambda_0 t, t)$ so that the resulting system has an isolated singularity at $u = (0, 0)$ with corresponding double eigenvalue $\lambda = 0$. Then system (1) is obtained by expanding the flux functions of this transformed system in Taylor series about $(0, 0)$ and neglecting higher order terms.

System (1) can be reduced further by a nonsingular linear change of dependent variables. Two systems related by such a transformation S are isomorphic in the sense that $Su(x, t)$ is a weak solution of the transformed system if and only if $u(x, t)$ is a weak solution of the original system. Since the nonsingular transformation S contains four free parameters and since system (1) contains six parameters, we expect to find a two parameter family of isomorphism classes for system (1). Thus, we look for representatives of the isomorphism classes in a normal form containing two free parameters [8]. In what we consider to be a breakthrough, Shearer and Schaeffer showed in [17] that when system (1) is hyperbolic, there is a nonsingular linear change of dependent variables which transforms system (1) into

$$(3) \quad \begin{aligned} u_t + \frac{1}{2} \{au^2 + 2buv + v^2\}_x &= 0, \\ v_t + \frac{1}{2} \{bu^2 + 2uv\}_x &= 0. \end{aligned}$$

System (3) depends on two free parameters a and b and can be taken as a normal form for the hyperbolic quadratic systems (1). It is also shown in [3, 17] that the integral curves of (3) fall into four nonisomorphic classes depending on the parameters a and b . These classes define four regions in the a, b -plane which are referred to as Regions I-IV.

The regions are determined by the number of lines which form the Hugoniot locus of the origin, as well as the direction of increase of the appropriate eigenvalue on these lines. In Regions I-III, the Hugoniot locus consists of three distinct lines, while in Region IV it consists of one line. Specifically, the boundary between Regions I and II is given by $a = \frac{3}{4} b^2$, the boundary between Regions II and III is given by $a = 1 + b^2$, and

the boundary between Regions III and IV is given by $4\{4b^2 - 3(a - 2)\}^3 = \{16b^3 + 9(1 - 2a)b\}^2$ [cf. 17]. The structure of solutions in each region is simplest when $b = 0$ since then solutions have both up-down symmetry $[(u, -v)$ satisfies (3) if and only if (u, v) does] and left-right symmetry $[(u(x, t), v(x, t))$ satisfies (3) if and only if $(-u(-x, t), v(-x, t))$ does]. We call the systems with $b = 0$ symmetric. (An additional simplifying feature of the symmetric systems is that the lines on which genuine nonlinearity fails coincide with the Hugoniot locus of the origin.)

The present paper is the first of a series in which we give the solution of the Riemann problem

$$(4) \quad \underline{u}(x, 0) = \begin{cases} \underline{u}_L \equiv (u_L, v_L), & x < 0 \\ \underline{u}_R \equiv (u_R, v_R), & x > 0 \end{cases}$$

for the symmetric systems in Regions II-IV of Schaeffer and Shearer [17]. There are new features in these regions that do not occur in Region I [cf. 18]. First, a type of shock which we call compressive appears in solutions of the Riemann problem, and the existence of such shocks is necessary to ensure (in the x, t -plane) the continuous dependence of solutions on \underline{u}_L and \underline{u}_R [cf. 6, 7, 9, 21]. Schaeffer [25] noted that the compressive shocks perturb to a 1-shock followed by a 2-shock. This fact is manifested in the triple shocks which appear in the solutions.

A second feature that occurs in Regions II-IV that does not occur in Region I is the following: in Regions II-IV there are lines on which $\lambda = 0$, whereas in Region I, $\lambda = 0$ if and only if $\underline{u} = 0$. These lines play a central role both in the classification as well as in the structure of Riemann problem solutions. In fact, the lines $\lambda = 0$ give a geometric interpretation for the boundaries between the Regions I-III located by Schaeffer and Shearer. (See the Appendix and Figure 8.) Also, in Regions II-IV the structure of the shock types on the Hugoniot locus of a point \underline{u} changes as \underline{u} crosses a line $\lambda = 0$; this entails a corresponding change in the structure of the solutions of the Riemann problem. The reason for the change in shock type is that the state \underline{u} on the line $\lambda = 0$ can be joined to the state $-\underline{u}$ by a two-sided contact discontinuity.

Our construction of the solutions of the Riemann problem is based on a numerical construction of the Hugoniot loci together with the structure of the integral curves obtained from [17]. Some analysis is presented to justify the salient features of the solutions obtained. In particular, our analysis uses an explicit parameterization of the Hugoniot locus (see the Appendix). The fact that the Hugoniot locus is star-like with respect to the left state was pointed out by Shearer [24].

In the present paper we give the solution of the Riemann problem for system (3) in the parameter range

$$(5) \quad a > 2, \quad b = 0.$$

This condition specifies the symmetric systems in Region IV. We present the solution in Section 3 by means of a series of diagrams (Figures 7A-F). Because of up-down symmetry, we give the solutions only for u_L in the lower half-plane. The solution diagrams are qualitatively the same for all u_L in the sector

$$A_1 = \{u : \theta_* < \theta_L < 0\},$$

and are qualitatively the same for all u_L in the sector

$$A_2 = \{u : -\pi < \theta_L < \theta_*\},$$

where

$$\theta_L = \arctan\left(\frac{v_L}{u_L}\right),$$

$$\theta_* = \arctan(-\sqrt{a}).$$

This separation angle θ_* depends on a , and the ray $\theta = \theta_*$ is the ray (in the lower half-plane) on which $\lambda_1 = 0$. The solution consists of a 1-composite wave followed by a 2-composite wave in analogy with the local solutions for strictly hyperbolic systems [cf. 11,14]. Here, however, the wave curves have a different structure: as in [6,7,9,21], intermediate solution states do not depend continuously on the data due to the appearance of compressive shocks. However, as in [6,7,9,21], continuous dependence on u_L and u_R is ensured in x,t -space because of the coincidence of shock speeds in the compressive

shocks. In this paper we construct explicitly for each state \underline{u} the 1-wave curve $\omega_1(\underline{u})$ and the 2-wave curve $\omega_2(\underline{u})$ such that the following theorem holds:

THEOREM: For each pair of states \underline{u}_L and \underline{u}_R , there exists an intermediate state $\underline{u}_M \in \omega_1(\underline{u}_L)$ such that $\underline{u}_R \in \omega_2(\underline{u}_M)$ and the solution of the Riemann problem (3), (4), (5) consists of the 1-wave from \underline{u}_L to \underline{u}_M followed by the 2-wave from \underline{u}_M to \underline{u}_R . Moreover, the solution is unique in x, t -space and depends continuously on \underline{u}_L and \underline{u}_R .

In Figures 7A-F, pictorial solutions of the Riemann problem are presented in which the state \underline{u}_L is fixed, and an arbitrary point in the diagram represents \underline{u}_R . The waves in the solution of the Riemann problem are determined by the path from \underline{u}_L to \underline{u}_R which consists of (portions of) wave curves and is indicated by the arrows.

In Section 2 we discuss the wave curves ω_1 and ω_2 . In Section 3 we describe the diagrams in Figures 7A-E individually, and in Section 4 we verify the salient features of these diagrams. General properties of system (1) are stated in the Appendix and are referred to throughout. The Appendix also contains the interpretation of Regions I-III in terms of the lines $\lambda = 0$. These are depicted in Figures 8A-D.

§2. Elementary Waves

The integral curves of the eigenvector fields of the Jacobian $A(u)$ determine the rarefaction waves of system (2). The Hugoniot loci $H(u_L)$ for states u_L determine the shock waves of system (2), and are given by [20]

$$H(u_L) \equiv \{u : s(u - u_L) = f(u) - f(u_L) \text{ for some } s \in \mathbb{R}\}.$$

The general solution of the Riemann problem which we construct is obtained by composing rarefaction waves and shock waves. Because the flux functions in (1) are homogeneous quadratics, the integral curves and Hugoniot loci for system (1) have the following scaling property: if Γ is an integral curve or Hugoniot locus through u_L , then $c\Gamma$ is the corresponding integral curve or Hugoniot locus through cu_L , $c \neq 0$. The eigenvalues and shock speeds scale similarly. Thus the integral curves and Hugoniot locus through u_L determine the corresponding integral curves and Hugoniot locus for each state u satisfying $\theta = \theta_L$ where

$$\theta = \arctan\left(\frac{v}{u}\right).$$

For the Hugoniot loci, the up-down and left-right symmetries imply that if $u_R \in H(u_L)$, then $\bar{u}_R \in H(\bar{u}_L)$ and $\hat{u}_R \in H(\hat{u}_L)$ where $\bar{u} = (u, -v)$ and $\hat{u} = (-u, v)$. Thus, the reflection of a Hugoniot curve about either the u - or v -axis is also a Hugoniot curve. In terms of wave speeds and shock speeds, the symmetries of (3) when $b = 0$ yield the following relationships:

$$(2.1) \quad \lambda_p(u) = \lambda_p(\bar{u}) = -\lambda_{\hat{p}}(\hat{u}), \quad p = 1, 2$$

$$(2.2) \quad \sigma(u_L, u_R) = \sigma(\bar{u}_L, \bar{u}_R) = \sigma(\hat{u}_L, \hat{u}_R)$$

where \hat{p} denotes the other family.

In Table 1 we label nine types of shocks according to the inequalities that hold between the characteristic speeds of u_L , u_R and the shock speed $\sigma(u_L, u_R)$. (Obvious inequalities are omitted.) Since the two wave speeds λ_1 and λ_2 assigned to each state are ordered, Table 1 gives the totality of shock types that can occur in any 2×2 system (2). In the case of the symmetric systems (3), the formulas (2.1) and (2.2) imply the following symmetries for shock types: if $u_R \in H(u_L)$, then the shock type of

$\langle \bar{u}_L, \bar{u}_R \rangle$ will be the same as the shock type of $\langle u_L, u_R \rangle$; and the shock type of $\langle \hat{u}_L, \hat{u}_R \rangle$ will be what we call the inverse of the shock type of $\langle u_L, u_R \rangle$. Here, the inverse shock type is obtained by reversing the inequalities which hold between the shock speed and each wave speed to the right and left of the shock and also by interchanging the families 1 and 2. Therefore [cf. Table 1], 1-shock and 2-expansive are inverses; 2-shock and 1-expansive are inverses; compressive and expansive are inverses; right transport and left transport are inverses; and crossing is its own inverse. Thus in the symmetric cases, all Hugoniot curves and shock types are determined by the Hugoniot curves and shock types for states in a single quadrant of the u, v -plane. Among the above shock types, some occur in the solutions of system (3) that do not occur for strictly hyperbolic systems. For the symmetric systems of classes II-IV, there are three types of shocks that appear in solutions: 1-shocks, 2-shocks, and compressive shocks which are defined by [cf. Table 1]

$$\lambda_1(u_R) < \lambda_2(u_R) < \sigma(u_L, u_R) < \lambda_1(u_L) < \lambda_2(u_L) .$$

We refer to any of the three types of shocks above as admissible. We refer to shocks of other types as inadmissible. (We note that the transport shocks are the only types that do not appear in Hugoniot loci of the symmetric systems in classes II-IV.) Our scheme for labeling shock types in Figures 3-7 is described in the legend which precedes the diagrams.

1-SHOCK:	$s < \lambda_1(u_L)$ $\lambda_1(u_R) < s < \lambda_2(u_R)$
1-EXPANSIVE:	$\lambda_1(u_L) < s < \lambda_2(u_L)$ $s < \lambda_1(u_R)$
2-SHOCK:	$\lambda_1(u_L) < s < \lambda_2(u_L)$ $\lambda_2(u_R) < s$
2-EXPANSIVE:	$\lambda_2(u_L) < s$ $\lambda_1(u_R) < s < \lambda_2(u_R)$
COMPRESSIVE:	$\lambda_2(u_R) < s < \lambda_1(u_L)$
EXPANSIVE:	$\lambda_2(u_L) < s < \lambda_1(u_R)$
CROSSING:	$\lambda_1(u_L) < s < \lambda_2(u_L)$ $\lambda_1(u_R) < s < \lambda_2(u_R)$
RIGHT TRANSPORT:	$s < \lambda_1(u_L)$ $s < \lambda_1(u_R)$
LEFT TRANSPORT:	$\lambda_2(u_L) < s$ $\lambda_2(u_R) < s$

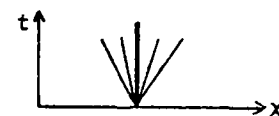
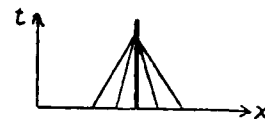
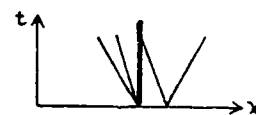
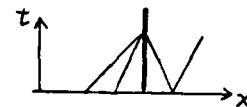


TABLE 1

In the diagrams above, the centerline denotes a shock in x, t -space. The lines to the left and right of the shock are characteristic lines, and indicate the relationship between the shock speed and the wave speeds on the left and right.

§2.1. Integral Curves

For system (3) with parameter values (5),

$$\Lambda(u) = \begin{bmatrix} au & v \\ v & u \end{bmatrix},$$

and the integral curves are depicted in Figure 1 [3,17]. We call the integral curves associated with the eigenvalues $\lambda_1(u) < \lambda_2(u)$ the 1-, 2-integral curves. For example, when $a = 3$ the integral curves are the one-parameter family of parabolas

$$u - u_0 = -\frac{1}{4u_0} v^2,$$

where u_0 is the value at which the parabola crosses the u -axis. The u -axis is itself an integral curve for the symmetric systems $b = 0$. For general $a > 2$, the integral curves are parabola-like and the 1-integral curves open to the left, the 2-integral curves open to the right. The arrows in Figure 1 indicate the direction in which the corresponding eigenvalues increase. We define the i -rarefaction curve $R_i(u_L)$, $i = 1, 2$, to be the set of states u_R such that the solution of the Riemann problem (3), (4) is a pure i -rarefaction wave (see [14]); $R_i(u_L)$ is thus the connected portion of the i -integral curve through u_L consisting of those states u for which λ_i increases along the curve from u_L to u .

§2.2. The Hugoniot Locus

For system (3) with parameter values (5), the qualitative shape of the Hugoniot locus $H(u_L)$ is as follows: for $u_L = 0$, $H(u_L)$ is the u -axis; for u_L on the u -axis, $H(u_L)$ consists of an ellipse together with the u -axis; and for u_L off the u -axis, $H(u_L)$ perturbs to a closed loop surrounding the origin with two tails which are asymptotic at infinity to opposite ends of the horizontal line

$$v = \frac{a}{a-2} v_L.$$

These properties follow from the explicit parameterization of the Hugoniot locus given in the Appendix and are depicted in Figures 3A-F. The shock type is also indicated. We

let $S_p(u_L)$ denote that portion of $H(u_L)$ consisting of 1-shocks for $p = 1$, 2-shocks for $p = 2$, and compressive shocks for $p = c$.

The subset $S_c(u_L)$ is non-empty for u_L in the sector A_1 , and $S_c(u_L)$ is empty for u_L in the sector A_2 . Moreover, $S_1(u_L)$ has two disconnected components for $u_L \in A_1$ but only one for $u_L \in A_2$. This explains why the ray $\theta = \theta_*$ is the boundary across which the qualitative structure of the solution diagrams changes.

We note in Figure 3B that B_L, D_L are the points at which

$$\sigma(u_L, B_L) = \lambda_1(u_L) = \sigma(u_L, D_L) ;$$

in Figures 3A, B, C, D that C_L is the point at which

$$\lambda_2(C_L) = \sigma(u_L, C_L) ;$$

and in Figure 3C that

$$\lambda_1(u_L) = \sigma(u_L, C_L) = \lambda_2(C_L) \quad (= 0) .$$

§2.3. Composite Waves

The solutions of the Riemann problem are compositions of pure rarefaction waves and pure shock waves. We refer to a Riemann problem solution consisting entirely of waves of one family as a composite wave of that family. The composite waves in the solutions of Riemann problems for system (3) in parameter range (5) are of two types: a 1-rarefaction wave followed by a 1-shock wave and a 2-shock wave followed by a 2-rarefaction wave. In each case, the speed of the shock equals the speed of the adjacent rarefaction wave. We call these 1RS- and 2SR-composite waves, respectively. (See Figure 4. The letters in Figure 4 refer to states appearing in Figure 5 where the composite waves may be viewed in state space.)

For each u we define the 1-composite curve $C_1(u)$. In Figure 5 a 1RS-composite wave with left state u is a wave consisting of a 1-rarefaction wave from u to $F \in R_1(u)$ followed by a 1-shock from F to $D \in S_1(F)$ such that $\sigma(F, D) = \lambda_1(F)$. Such a shock exists if and only if F lies on that portion of $R_1(u)$ in Sector A_1 . We define the 1-composite curve $C_1(u)$ to be the set of all such states D . Thus, the 1-

composite curve $C_1(u_*)$ is maximal for u_* on the boundary ray $\theta = \theta_*$ in the sense that

$$C_1(u_*) = C_1(u) \text{ for } u \in R_1(u) ,$$

$$C_1(u_*) \supseteq C_1(u) \text{ for } u \in R_1(u_*) ,$$

for example, in Figure 5,

$$C_1(u) = C_1(u_*) = [EDC_*] \text{ and } C_1(F) = [ED] \subseteq C_1(u_*) .$$

(Here, letters enclosed by brackets denote the curves that connect the corresponding points in the Figures.) In fact, as F moves from E to u_* along $R_1(u_*)$, D moves from E to C_* along $C_1(u_*)$. Moreover,

$$C_* = -u_* ,$$

and

$$\sigma(u_*, C_*) = \lambda_2(C_*) = \lambda_1(u_*) = 0 .$$

For each curve Γ we define the 2-boundary curve based on Γ . In Figure 5, a 2SR-composite wave with left state u is a wave consisting of a 2-shock wave from u to $C \in S_2(u)$ followed by a 2-rarefaction wave from C to any $G \in R_2(C)$ such that $\sigma(u, C) = \lambda_2(C)$. Such a shock exists if and only if u lies on that portion of Γ in sector A_2 . We define the 2-boundary curve to be the set of all such states C . For example, in Figure 5, $[C_*C_0]$ is the 2-boundary curve based on $[u_*u_0]$. Thus, for left states u on $\Gamma = [u_*u_0]$, the states C on the 2-boundary curve $[C_*C_0]$ are transition states between 2-shock waves and 2-composite waves.

§2.4. Wave Curves

We define the wave curve $W_i(u_L)$, $i = 1, 2$, to be the set of states u_R for which the solution of the Riemann problem (2), (4) is a pure composite wave of the appropriate family. Thus, (see Figures 6A, B)

$$W_1(u_L) = S_1(u_L) \cup R_1(u_L) \cup C_1(u_L) ,$$

and

$$W_2(u_L) = R_2(u_L) \cup S_2(u_L) \cup R_2(C) ,$$

where C is the endpoint of $S_2(\underline{u}_L)$ at which $\sigma(\underline{u}_L, C) = \lambda_2(C)$. The geometry of these curves is indicated in Figure 6 for \underline{u}_L in sectors A_1 and A_2 .

§3. Solution of the Riemann Problem

For each \underline{u}_L we describe the solution of the Riemann problem for arbitrary \underline{u}_R by means of a diagram. In Figures 7B and D we present a diagram of the solution of the Riemann problem for representative values of \underline{u}_L in sectors A_1 and A_2 in each of which the solution diagrams are qualitatively the same. For completeness and in order to see clearly the continuous dependence of solutions on \underline{u}_L , we also give in Figures 7A,C,E the solution diagrams for typical values of \underline{u}_L on the boundaries of sectors A_1 and A_2 , i.e., for \underline{u}_L on the rays $\theta = 0$, $\theta = \theta_*$, and $\theta = -\pi$. In Figures 7A-D, the representative values \underline{u}_L are chosen to lie on the 1-integral curve through the fixed state E on the positive u -axis. In Figure 7F we present the solution for $\underline{u}_L = 0$.

The solution of the Riemann problem consists of a 1-wave with left state \underline{u}_L and right state \underline{u}_M followed by a 2-wave with left state \underline{u}_M and right state \underline{u}_R . We find the intermediate state in the Figures as follows: given \underline{u}_R , follow the 2-wave curve backwards from \underline{u}_R (opposite the direction of the arrows) until you reach a point \underline{u}_M in the 1-wave curve $W_1(\underline{u}_L)$. The state \underline{u}_M so constructed satisfies $\underline{u}_R \in W_2(\underline{u}_M)$ and defines the waves in the solution. This procedure is not well-defined when $\{\underline{u}_L, \underline{u}_M, \underline{u}_R\}$ form a triple shock:

$$(3.1) \quad u_M \in H(\underline{u}_L), \underline{u}_R \in H(\underline{u}_L), \underline{u}_R \in H(\underline{u}_M),$$

and

$$(3.2) \quad \sigma(\underline{u}_L, \underline{u}_M) = \sigma(\underline{u}_L, \underline{u}_R) = \sigma(\underline{u}_M, \underline{u}_R).$$

Triple shocks occur when $\underline{u}_R \in S_C(\underline{u}_L)$ or when \underline{u}_R is in the triple shock curve (which will be defined in each Figure). When the procedure is not well-defined, there are two such intermediate states \underline{u}_M ; however, the two solutions obtained are identical in x, t -space because then all shock speeds in the problem are equal. This ensures continuous dependence of the solution on the initial data \underline{u}_L and \underline{u}_R .

We now discuss the solution diagrams 7A-E individually.

§3.1. Solution for $\theta_L = 0$

In Figure 7A, $u_L \in E$ lies on the u -axis to the right of the origin. In this case the Hugoniot locus $H(u_L)$ consists of the u -axis together with the ellipse E depicted. The vertices of E on the major axis are u_L and $C_L \equiv -\frac{a}{a-2}u_L$. The point A is given by

$$(3.3) \quad A = -\frac{a-2}{a}u_L.$$

Point A is the limit of intersections of $S_2(u)$ with the u -axis as u tends to u_L through states with $v \neq 0$. The solution of the Riemann problem consists of a 1-shock with left state u_L and right state $u_M \in S_1(u_L)$ followed by a 2-rarefaction wave if u_R lies outside E , and followed by a 2-shock if u_R lies inside E . The u -axis between C_L and A is $S_C(u_L)$ where triple shocks occur in pairs. In fact, for each $v \in E$, $v \neq u_L$, there exists a unique $u \in S_C(u_L)$ such that both $\{u_L, v, u\}$ and $\{u_L, \bar{v}, u\}$ are triple shocks of the same speed. (Here \bar{v} is the reflection of v in the u -axis.) Thus for $u_R \in S_C(u_L)$, the solution of the Riemann problem is unambiguous in the x, t -plane.

§3.2. Solution for $\theta_* < \theta_L < 0$

In Figure 7B, u_L lies in the sector A_1 . The Hugoniot locus $H(u_L)$ is depicted by the thin solid curve through u_L . Here

$$S_1(u_L) = [\infty K_L u_L] \cup [D_L C_L],$$

$$R_1(u_L) = [u_L E],$$

$$C_1(u_L) = [E D_L],$$

and the union of these three curves is the 1-wave curve $W_1(u_L)$. Moreover,

$$S_C(u_L) = [C_L B_L],$$

and the triple shock curve is $[B_L A]$.

For u_R on either of these latter two curves, triple shocks occur: for $R \in S_C(u_L)$ there is a pair of triple shocks $\{u_L, P, R\}$ and $\{u_L, Q, R\}$ with all shock

speeds being equal; for $R \in [B_L A]$, a single triple shock occurs. Hence, continuous dependence is ensured.

The curve $[C_L C'^\infty]$ is the 2-boundary curve based on $[K_L u'^\infty]$, and 2SR-composite waves occur precisely when u_R lies "above" $[C_L C'^\infty]$ so that $u_M \in [K_L u'^\infty]$.

The states B_L and D_L satisfy

$$\sigma(u_L, B_L) = \sigma(u_L, D_L) = \sigma(D_L, B_L) = \lambda_1(u_L).$$

The state C_L is the point where $H(u_L)$ is tangent to a 2-integral curve. (See the Tangency Rule in the Appendix.) This implies that $\sigma(u_L, C_L) = \lambda_2(C_L)$ and that C_L is in, and marks the end of, the 2-boundary curve $[C_L C'^\infty]$. This insures continuous dependence near the point C_L .

For u_L in sector A_1 , the states B_L, D_L separate the states u_L, C_L on the portion of $H(u_L)$ consisting of the closed loop. As θ_L decreases to θ_* , B_L and D_L become coincident with C_L , and so both $S_C(u_L)$ and the disconnected portion $[D_L C_L]$ of $S_1(u_L)$ disappear. The fact that there exists a point at which $H(u_L)$ intersects the 1-composite curve $[ED_L]$ characterizes the states in A_1 .

§3.3. Solution for $\theta_L = \theta_*$

In Figure 7C, $u_L = u_*$ lies on the line $\theta = \theta_*$. The Hugoniot locus $H(u_L)$ is depicted by the thin solid curve through u_L . Here

$$S_1(u_L) = [u_L u'^\infty],$$

$$R_1(u_L) = [u_L E],$$

and

$$C_1(u_L) = [ED_L].$$

The union of these three curves is $W_1(u_L)$. In this case

$$S_C(u_L) = [C_*],$$

and the curve $[C_* A]$ is the triple shock curve.

The curve $[C_* C'^\infty]$ is the 2-boundary curve based on $[u_L u'^\infty]$, and 2SR-composite waves occur precisely when u_R lies "above" $[C_* C'^\infty]$ so that $u_M \in [u_L u'^\infty]$. Note that

$C_* = -u_L$ is the point where $H(u_L)$ is tangent to a 2-rarefaction curve, and also that

$$\sigma(u_L, C_*) = \lambda_1(u_L) = \lambda_2(C_*) .$$

Thus $\theta = \theta_*$ is the ray where B_L , C_L and D_L are coincident.

§3.4. Solution for $-\pi < \theta_L < \theta_*$

In Figure 7D, u_L lies in sector A_2 . The Hugoniot locus $H(u_L)$ is depicted by the thin solid curve through u_L . Here

$$S_1(u_L) = [u_L u_*] ,$$

$$R_1(u_L) = [u_L FE] ,$$

and

$$C_1(u_L) = [EDC_*] .$$

The union of these three curves is $W_1(u_L)$. In this case

$$(3.4) \quad S_C(u_L) = \emptyset ,$$

and $[ABC_*]$ is the triple shock curve. Condition (3.4) characterizes the states in A_2 .

For $u_M \in [u_* EC_*]$, the solution consists of a 1-rarefaction wave taking u_L to u_* followed by the solution of the Riemann problem $\langle u_*, u_R \rangle$ given in Section 3.3. The curve $[C_* C_L \infty]$ is the 2-boundary curve with base curve $[u_L u_*]$, and again 2SR-composite waves occur precisely when u_R lies "above" the curve $[C_* C_L \infty]$ so that $u_M \in [u_L u_*]$.

Note that C_* is the end of the 1-composite curve in the sense that there do not exist 1-shocks with left states $u \in [u_L u_*]$ which have speed $\lambda_1(u)$.

§3.5. Solution for $\theta_L = -\pi$

In Figure 7E, u_L lies on the negative u -axis. The Hugoniot locus consists of the u -axis together with the ellipse E depicted. The vertices of E on the major axis are

$$u_L \text{ and } G = -\left(\frac{a}{a-2}\right) u_L , \text{ and}$$

$$S_1(u_L) = [u_L] ,$$

and

$$R_1(u_L) = [u_L 0] .$$

The union of these two curves is $W_1(u_L)$. Here

$$C_1(u_L) = S_c(u_L) = \emptyset,$$

and the solution of the Riemann problem consists of a 1-wave followed by a 2-rarefaction wave. The solution for $u_L = 0$ is similar and given in Figure 7F.

§4. Justification

The solution of the Riemann problem presented in Section 3 is based on the assumptions that the integral curves and Hugoniot loci have the qualitative features discussed in Section 2. The relevant features of the integral curves which are required for our analysis are verified in [3,17]. The features of $H(u_L)$ (including shapes and locations of shock types) have been verified numerically, using an explicit parameterization of $H(u_L)$ (see the Appendix). We here present analytical evidence which supports the results of these numerical computations. Note that for u_L off the u -axis, system (3) in parameter range (5) is strictly hyperbolic and genuinely nonlinear in a neighborhood of u_L , and so the local theory of Lax [11] applies in some neighborhood of u_L . We now discuss the global features of the Hugoniot loci depicted in Figures 3A-C.

Figure 3A: In this case u_L is on the positive u -axis. The Hugoniot locus $H(u_L)$ consists of the u -axis together with the ellipse E given by

$$(a-2)u^2 + 2u_L u + v^2 = au_L^2,$$

with center $-\frac{1}{(a-2)}u_L$. For $u = (u,0)$, we have (see the Appendix)

$$\sigma(u_L, u) = \frac{1}{2} a(u + u_L),$$

$$\{\lambda_1(u), \lambda_2(u)\} = \{au, u\} \text{ and } \{\lambda_1(u_L), \lambda_2(u_L)\} = \{au_L, u_L\},$$

which verifies the shock types on the axis, and verifies that the shock type changes at

$$u_L, C_L \equiv -\frac{a}{a-2}u_L, \text{ and } A \equiv -\frac{a-2}{a}u_L.$$

Figure 3B: In this case $u_L \in A_1$. The points B_L, C_L and D_L are points where a transition in shock type occurs. The existence of the point C_L where $H(u_L)$ is tangent to a 2-integral curve follows from the geometry of the integral curves. This tangency at C_L implies (see the Tangency Rule in the Appendix)

$$\lambda_2(C_L) = \sigma(u_L, C_L).$$

Note also that \bar{u}_L and $-u_L$ both lie on $H(u_L)$, and

$$\sigma(u_L, \bar{u}_L) = u_L,$$

$$\sigma(u_L, -u_L) = 0.$$

This is obtained from the Midpoint Rule or directly from the Rankine-Hugoniot condition (see the Appendix). Also the speed $\lambda_1(u_L)$ satisfies

$$0 < \lambda_1(u_L) = \frac{a+1}{2} u_L - \frac{1}{2} \sqrt{(a-1)^2 u_L^2 + 4v_L^2} < u_L = \sigma(u_L, \bar{u}_L),$$

where the left hand inequality is equivalent to $u \in A_1$. Thus the shock speed $\sigma(u_L, \bar{u}_L)$ is larger than $\lambda_1(u_L)$, but $\sigma(u_L, -u_L)$ is smaller than $\lambda_1(u_L)$; hence, there exists a point $D_L \in H(u_L)$ between \bar{u}_L and $-u_L$ at which $\sigma(u_L, D_L) = \lambda_1(u_L)$. Similarly,

$$u_0 \equiv \left(\frac{1}{a} \{ u_L - \sqrt{(a-1)^2 u_L^2 + a v_L^2} \}, 0 \right)$$

is the intersection of $H(u_L)$ with the negative u -axis, and satisfies (see Appendix)

$$\sigma(u_L, u_0) = u_L.$$

Therefore, there is a point B_L above the u -axis between $-u_L$ and u_0 at which

$$\sigma(u_L, B_L) = \lambda_1(u_L). \text{ Consequently, } \{u_L, B_L, D_L\} \text{ is a triple shock.}$$

Figure 3C: In this case $u_L = u_*$ is on the ray $\theta = \theta_*$. As θ_L decreases to θ_* in Figure 3B, $S_c(u_L)$ and the portion $[D_L C_L] \subseteq S_1(u_L)$ vanish. In fact,

$$\lambda_1(u_*) = \sigma(u_*, -u_*) = \lambda_2(-u_*) = 0,$$

indicating that the points B_L and D_L do indeed become coincident with $-u_*$ as θ_L decreases to θ_* . We also note that $\lambda_2(-u_*) = \sigma(u_*, -u_*)$ implies, by the Tangency Rule, that $H(u_*)$ is tangent to a 2-integral curve at $-u_*$ and thus $C_L = -u_*$.

APPENDIX

Here we list for reference several properties of the quadratic conservation laws (1) which are helpful in the study of the Riemann problem.

MIDPOINT RULE: For system (1), $u_R \in H(u_L)$ if and only if the line segment joining u_L to u_R is tangent to a p-integral curve at the midpoint of the segment. Moreover, in this case

$$(A.1) \quad \sigma(u_L, u_R) = \lambda_p \left(\frac{u_L + u_R}{2} \right).$$

Proof: Use the linearity of $\frac{\partial f}{\partial u}$ together with the general formula

$$s(u_R - u_L) = f(u_R) - f(u_L) = \left\{ \int_0^1 \frac{\partial f}{\partial u} (u_L + \tau(u_R - u_L)) d\tau \right\} \cdot (u_R - u_L).$$

TRIPLE SHOCK RULE: For system (2), suppose the states u_1, u_2 , and u_3 satisfy

$$(A.2) \quad u_1 \in H(u_2), u_2 \in H(u_3), u_3 \in H(u_1).$$

Then either u_1, u_2 and u_3 are colinear or else

$$(A.3) \quad \sigma(u_2, u_1) = \sigma(u_3, u_2) = \sigma(u_1, u_3).$$

Proof: Let $s_{ij} = \sigma(u_i, u_j)$. Then

$$s_{21}(u_2 - u_1) = f(u_2) - f(u_1),$$

$$s_{32}(u_3 - u_2) = f(u_3) - f(u_2),$$

$$s_{13}(u_1 - u_3) = f(u_1) - f(u_3).$$

Adding gives

$$(s_{21} - s_{13})(u_2 - u_1) + (s_{32} - s_{13})(u_3 - u_2) = 0,$$

and the result follows.

TANGENCY RULE: For system (3), assume that $u_L \notin H(0)$. Then the following statements are equivalent regarding $u \in H(u_L)$, $u \neq u_L$:

- (i) $H(u_L)$ is tangent to a p-integral curve at the point u .

(ii) $\dot{s} = 0$ at \underline{u} . (Dot denotes differentiation with respect to arc length along $H(\underline{u}_L)$.)

(iii) $\lambda_p(\underline{u}) = \sigma(\underline{u}_L, \underline{u})$.

Proof: Differentiate

$$s(\underline{u} - \underline{u}_L) = f(\underline{u}) - f(\underline{u}_L)$$

along $H(\underline{u}_L)$ to obtain

$$\dot{s}(\underline{u} - \underline{u}_L) + s\dot{\underline{u}} = A(\underline{u})\dot{\underline{u}},$$

or

$$(A.4) \quad [A(\underline{u}) - sI]\dot{\underline{u}} = \dot{s}(\underline{u} - \underline{u}_L).$$

Suppose $H(\underline{u}_L)$ is tangent to a p-integral curve. Then $\dot{\underline{u}}$ is a right eigenvector of A with eigenvalue λ_p so that (A.4) becomes

$$(A.5) \quad (\lambda_p - s)\dot{\underline{u}} = \dot{s}(\underline{u} - \underline{u}_L).$$

Since $\underline{u}_L \notin H(0)$, the line joining \underline{u}_L to \underline{u} is not tangent to $H(\underline{u}_L)$ at \underline{u} . Thus we conclude from (A.5) that $\dot{s} = 0$ and $s = \lambda_p$, so that (i) \Rightarrow (ii) and (i) \Rightarrow (iii). Now suppose (ii). Then (A.4) gives that $\dot{\underline{u}}$ is an eigenvector and $s = \lambda_p$ for $p = 1$ or 2 . Thus (ii) \Rightarrow (i) and (ii) \Rightarrow (iii). Finally suppose (iii): $s = \lambda_p(\underline{u})$. If $\dot{\underline{u}}$ is not parallel to the eigenvector \underline{x}_p of $A(\underline{u})$ and $\dot{s} \neq 0$ then, (A.4) implies that $\underline{u} - \underline{u}_L$ is parallel to \underline{x}_p , (the other eigenvector of $A(\underline{u})$). However, by the midpoint rule, $\underline{u} - \underline{u}_L$ is also tangent to an integral curve at $\frac{1}{2}(\underline{u}_L + \underline{u})$. But this contradicts the fact that if $\underline{u}_L \notin H(0)$, then every line through \underline{u}_L is tangent exactly once to an integral curve. Consequently, $\dot{\underline{u}}$ is tangent to \underline{x}_p at \underline{u} , and hence $\dot{s} = 0$. Thus (iii) \Rightarrow (i) and (iii) \Rightarrow (ii).

EIGENVALUES AND SHOCK SPEEDS: For system (3) with $b = 0$, the eigenvalues are

$$\lambda_{1,2}(\underline{u}) = \frac{1}{2} \left\{ (a+1)u \pm \sqrt{(a-1)^2 u^2 + 4v^2} \right\}.$$

In addition, if $\underline{u}_R \in H(\underline{u}_L)$, then the Rankine-Hugoniot condition gives

$$\sigma(\underline{u}_L, \underline{u}_R) = \frac{u_R v_R - u_L v_L}{v_R - v_L} \quad (v_R \neq v_L).$$

SPECIAL POINTS ON $H(u_L)$: For system (3) with $b = 0$,

$$-u_L \in H(u_L) \text{ with } \sigma(u_L, -u_L) = 0,$$

and

$$\bar{u}_L \in H(u_L) \text{ with } \sigma(u_L, \bar{u}_L) = u_L.$$

Moreover, $H(u_L)$ crosses the u -axis at the points

$$u \equiv \left(\frac{1}{a} \{ u_L \pm \sqrt{(a-1)^2 u_L^2 + a v_L^2} \}, 0 \right),$$

and for such values of u ,

$$\sigma(u_L, u) = u_L$$

when $(a-1)^2 u_L^2 + a v_L^2 > 0$.

PARAMETRIZATION OF $H(u_L)$: For system (1), the Hugoniot locus $H(u_L)$ for $u_L \notin H(0)$ is parametrized by the angle φ of the polar coordinate system centered at u_L . Explicitly,

$$u \equiv u(\varphi) = u_L + R \cos \varphi,$$

$$v \equiv v(\varphi) = v_L + R \sin \varphi$$

where

$$R \equiv R(\varphi) = -2 \frac{a u_L + b v_L}{a \cos \varphi + b \sin \varphi},$$

$$\alpha \equiv \alpha(\varphi) = b_1 \sin^2 \varphi + (a_1 - b_2) \sin \varphi \cos \varphi - a_2 \cos^2 \varphi,$$

$$\beta \equiv \beta(\varphi) = c_1 \sin^2 \varphi + (b_1 - c_2) \sin \varphi \cos \varphi - b_2 \cos^2 \varphi.$$

For system (3) with $b = 0$, these become

$$\alpha \equiv (a-1) \sin \varphi \cos \varphi,$$

$$\beta \equiv 1.$$

In particular

$$\lim_{\varphi \rightarrow 0^-} |u| = \infty \quad \lim_{\varphi \rightarrow 0^-} v = \frac{a-2}{a} v_L$$

$$\lim_{\varphi \rightarrow -\pi^+} |u| = \infty \quad \lim_{\varphi \rightarrow -\pi^+} v = \frac{a-2}{a} v_L.$$

THE AXES $H(0)$: For system (1), the Hugoniot locus of the origin consists of the lines determined by the cubic equation

$$-a_2u^3 + (a_1 - 2b_2)u^2v + (2b_1 - c_2)uv^2 + c_1v^3 = 0.$$

For system (3), the equation is

$$-bu^3 + (a - 2)u^2v + 2buv^2 + v^3 = 0.$$

For $b = 0$, the equation is

$$(a - 2)u^2v + v^3 = 0.$$

THE LINES $\lambda = 0$: For system (1), the lines $\lambda = 0$ satisfy the quadratic equation

$$(a_1b_2 - b_1a_2)u^2 + (a_1c_2 - c_1a_2)uv + (b_1c_2 - c_1b_2)v^2 = 0.$$

For system (3), the equation is

$$(a - b^2)u^2 - buv - v^2 = 0.$$

For $b = 0$, the equation is

$$au^2 - v^2 = 0.$$

In particular, for $a > 0$ and $b = 0$, the set of states u for which $\lambda(u) = 0$ consists of the two lines through the origin with slopes

$$\frac{v}{u} = \pm \sqrt{a}.$$

The role of the lines $\lambda = 0$ in the classification of the integral curves: [see Figure 8]. In Region I, $\lambda = 0$ if and only if $u = 0$. The boundary between Regions I and II is the set of systems (3) for which the line $\lambda = 0$ coincides with a line in the Hugoniot locus of the origin. Crossing into Region II, this line splits into two lines, and systems in Region II are precisely those which satisfy the condition that the lines $\lambda = 0$ cut through the interiors of the four sectors closest to the u -axis which are determined by the Hugoniot locus of the origin. The boundary between Region II and Region III consists of the systems (3) for which the lines $\lambda = 0$ coincide with two lines other than the u -axis in the Hugoniot locus of the origin. And finally, the systems in Region III are characterized by the condition that the lines $\lambda = 0$ cut through the interiors of the two middle sectors determined by the Hugoniot locus of the origin.

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LEGEND

	1-rarefaction
	1-expansive shock
	1-shock
	2-rarefaction
	2-expansive shock
	2-shock (with or without arrows)
	1-composite (rarefaction followed by shock at characteristic speed)
	compressive shock
	crossing shock
	expansive shock
	2-boundary, triple shock curves
	Hugoniot locus of u_L and u-axis

NOTE 1: Arrows on rarefaction curves indicate the direction of increasing eigenvalue.

Arrows on shock curves indicate the direction of decreasing shock speed.

NOTE 2: 1- and 2-shocks in the Hugoniot locus of u_L are indicated by dashed lines supported by the solid line for the Hugoniot locus.

Figure Captions

Figure 1: Integral curves for the symmetric systems in Region IV; i.e., system (3) with $b = 0$, $a > 2$. (Family 1 is denoted by the thicker lines.)

Figure 2: The Sectors A_1, A_2 determined by the ray $\theta = \theta_*$ ($\lambda_1 = 0$).

Figures 3A-F: Hugoniot loci and shock types for \underline{u}_L in representative positions.

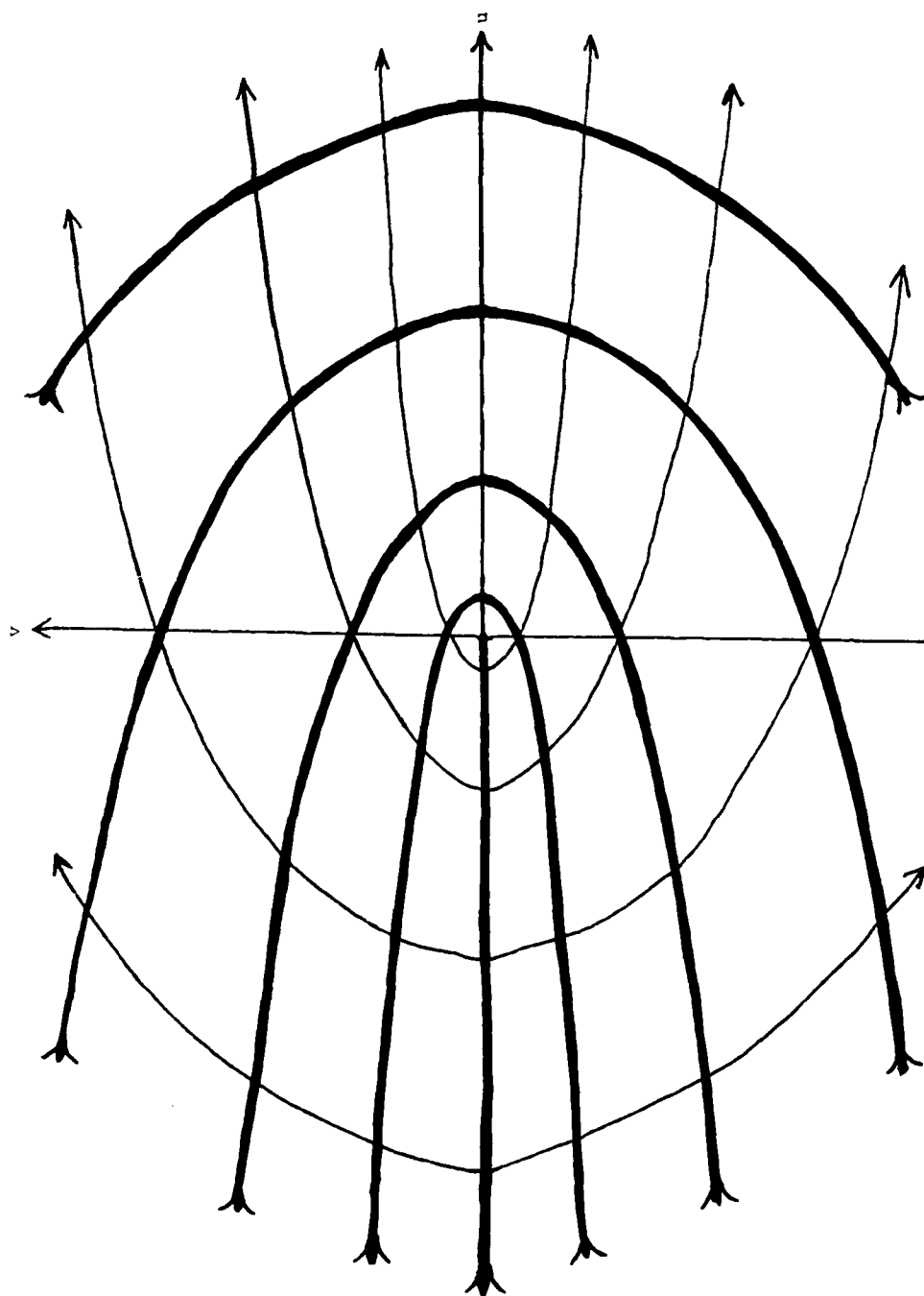


Figure 1

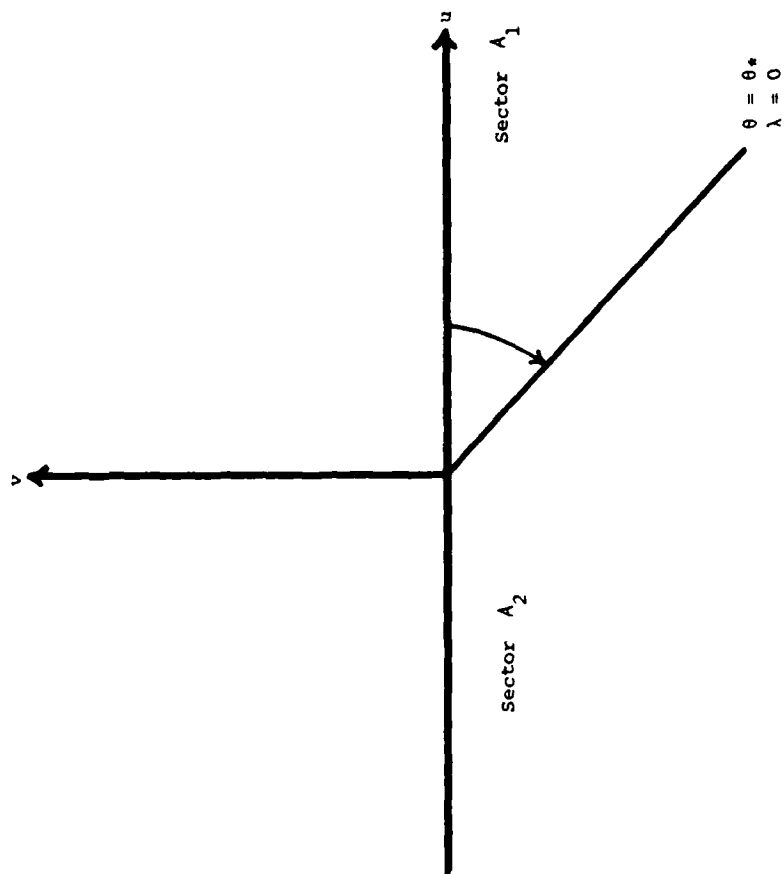


Figure 2

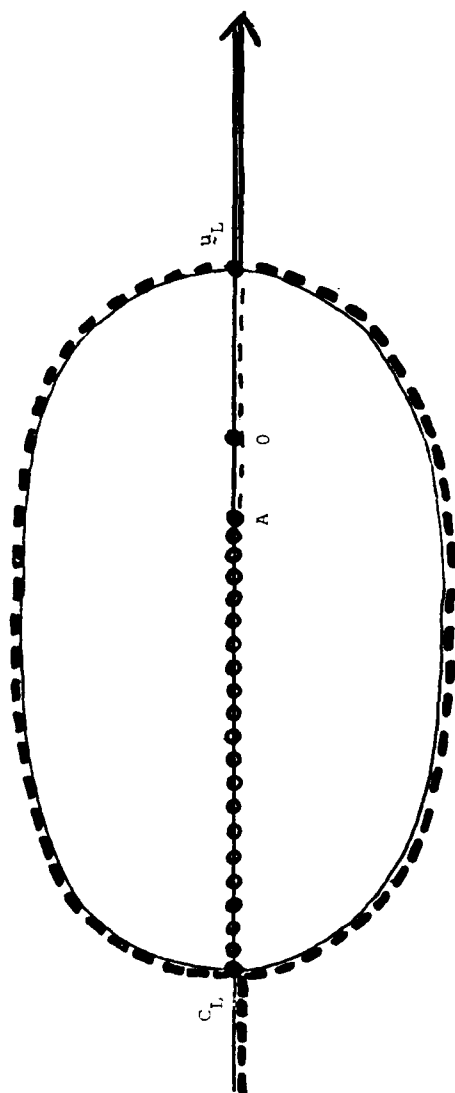


Figure 3A

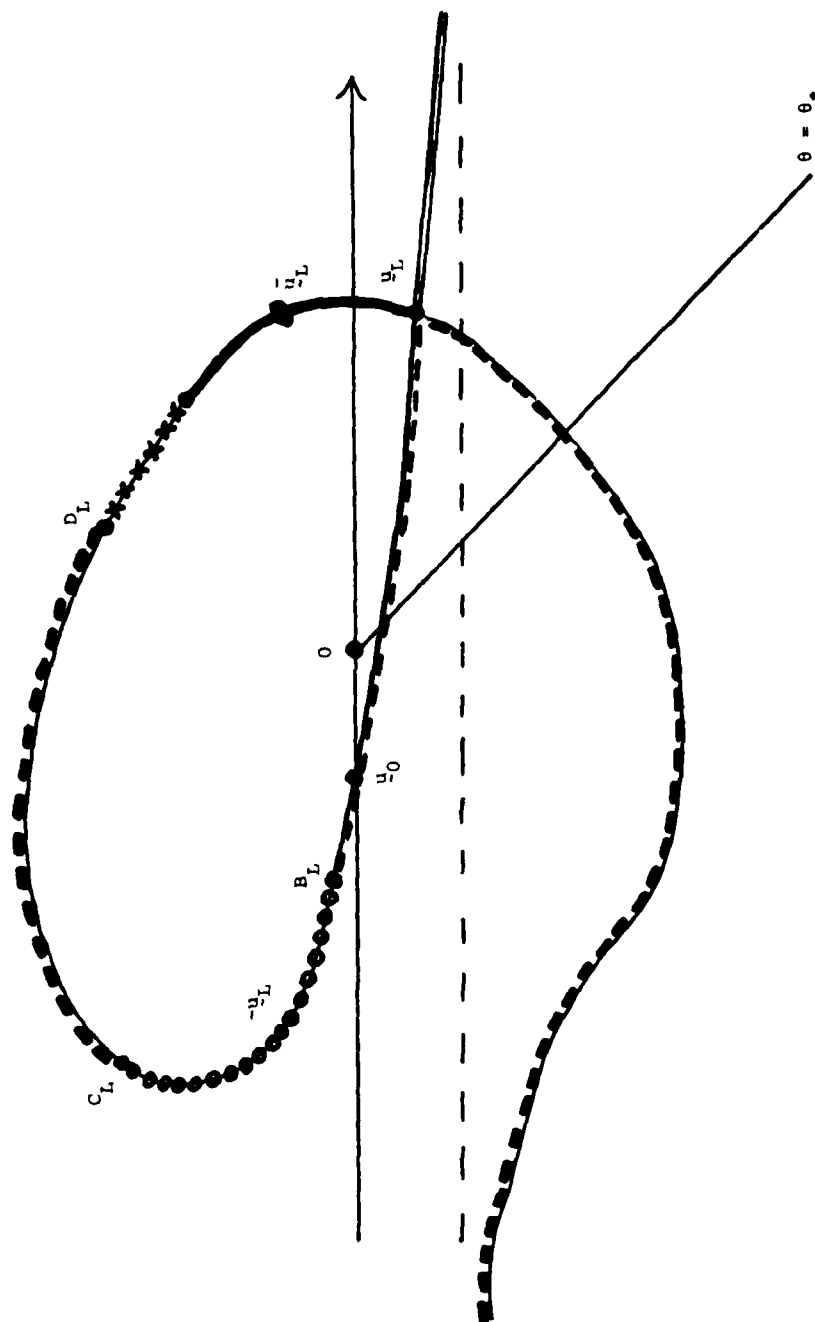


Figure 3B

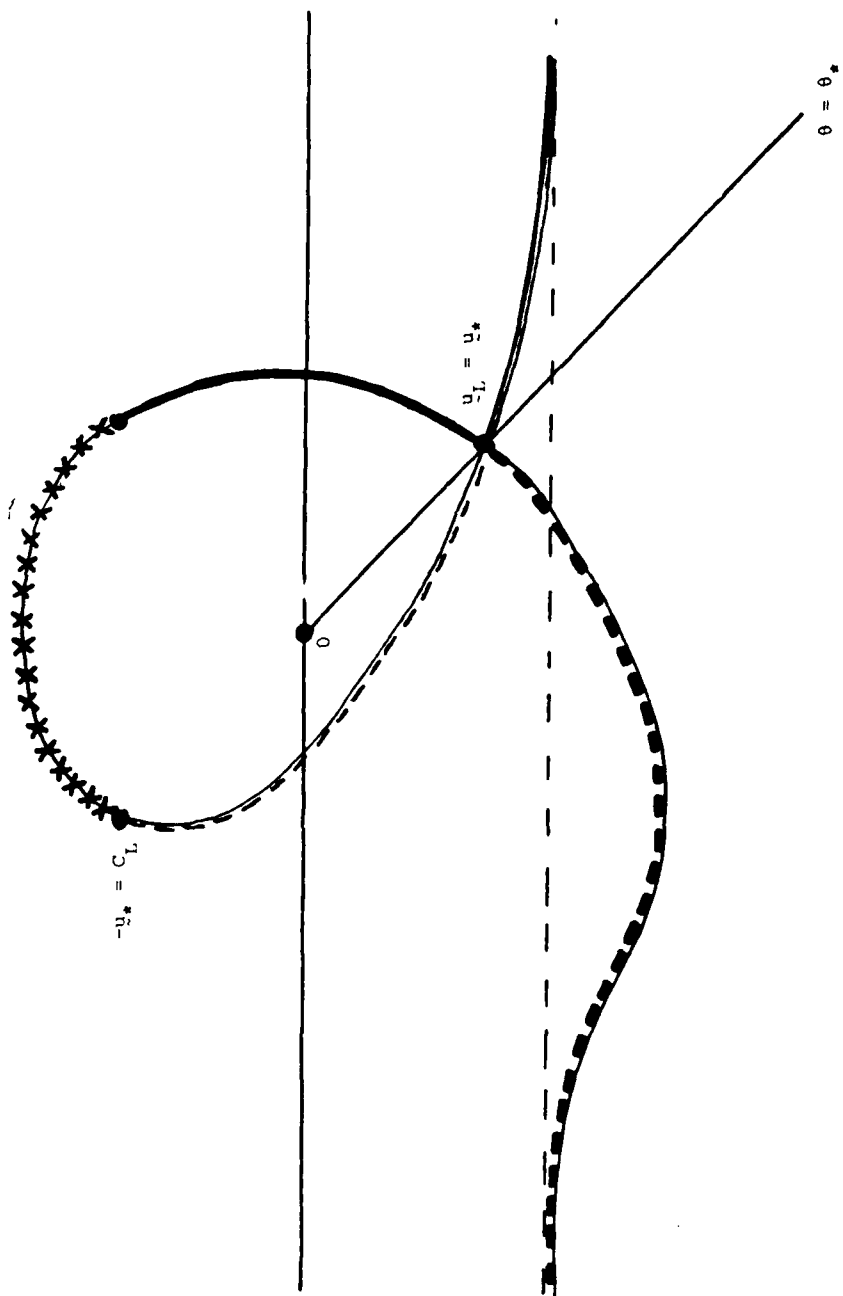


Figure 3C

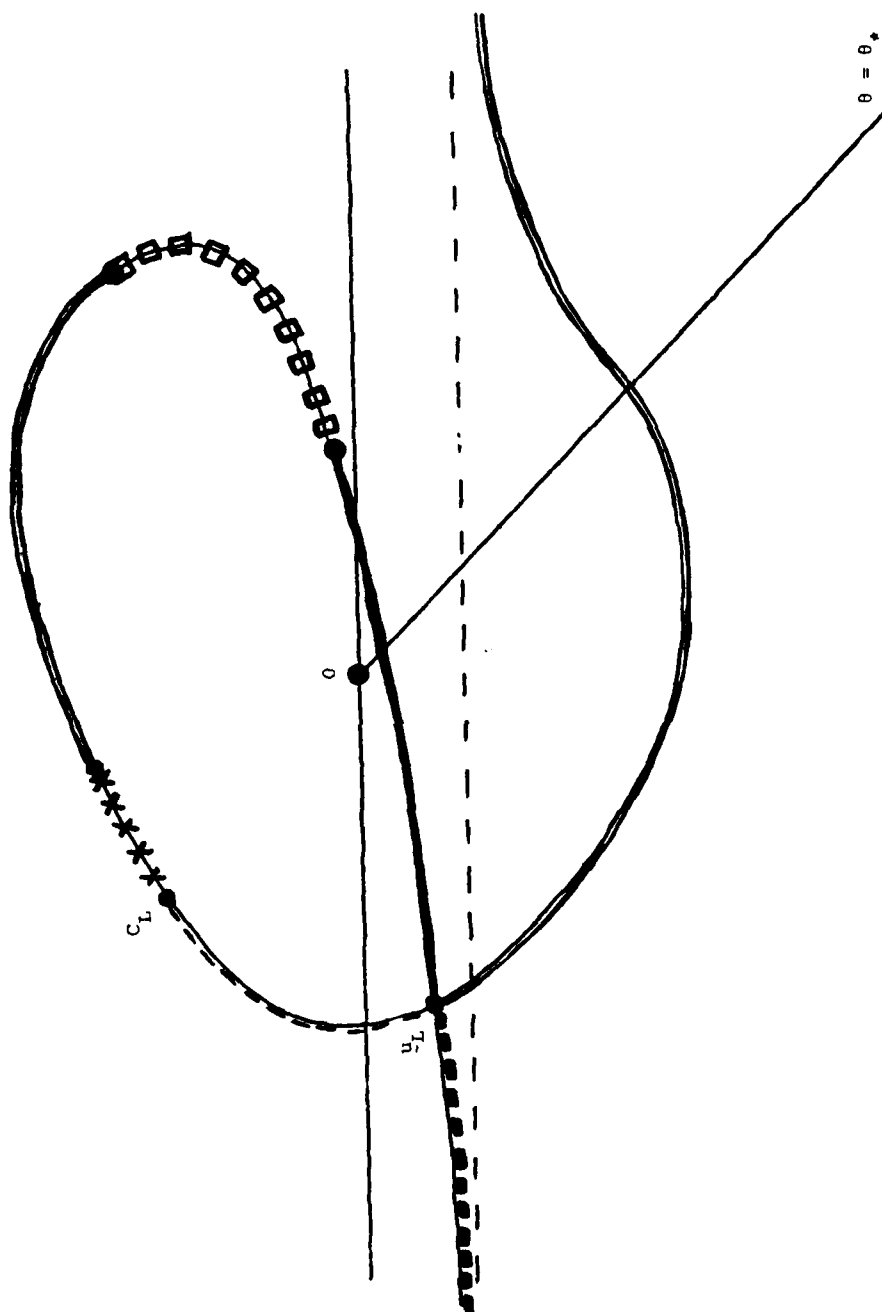


Figure 3D

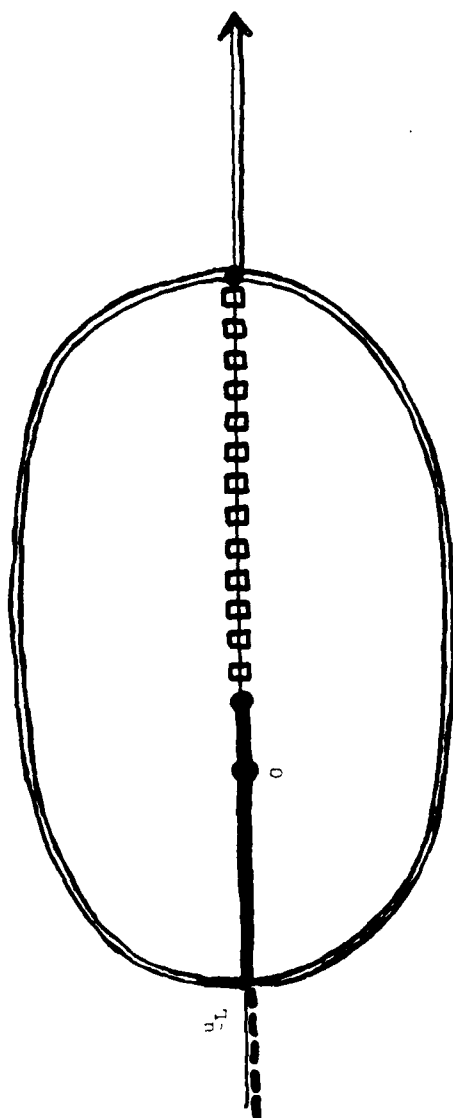


Figure 3E



$$u_L = 0$$

Figure 3F

Figure 4A: 1RS-composite wave in x, t -space.

Figure 4B: 2SR-composite wave in x, t -space.

Figure 5: Typical curves:

Rarefaction ($R_1(u) = \{uFE\}$),

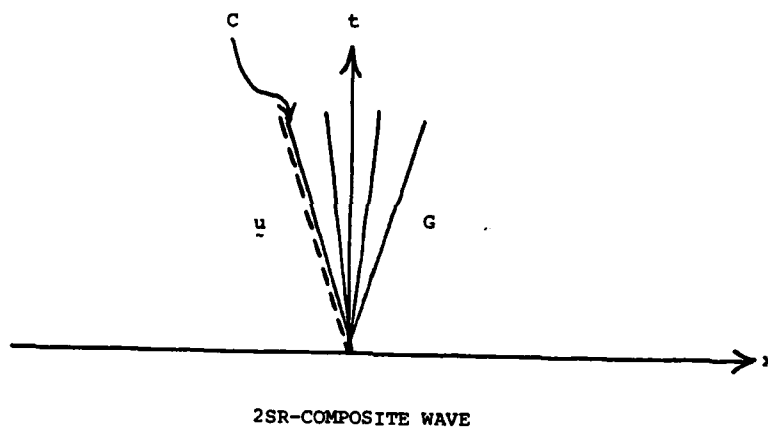
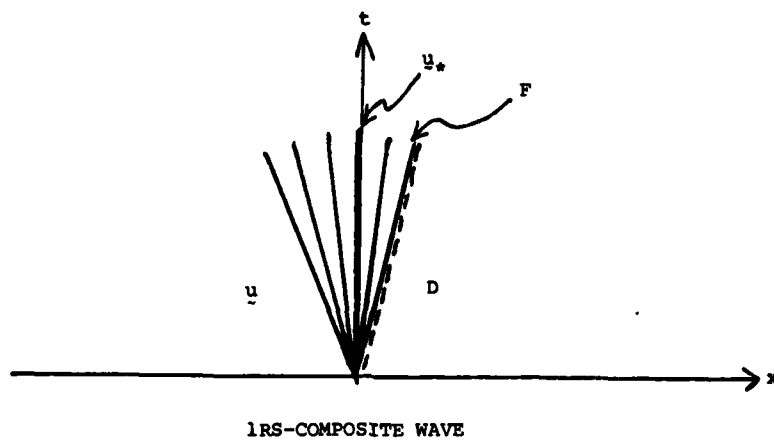
1-Composite ($C_1(F) = \{ED\}$),

2-Boundary ($\{=CC_*\}$),

Triple Shock ($\{ABC_*\}$).

Figure 6A: The wave curves for $u_L \in A_1$.

Figure 6B: The wave curves for $u_L \in A_2$.



Figures 4A, 4B

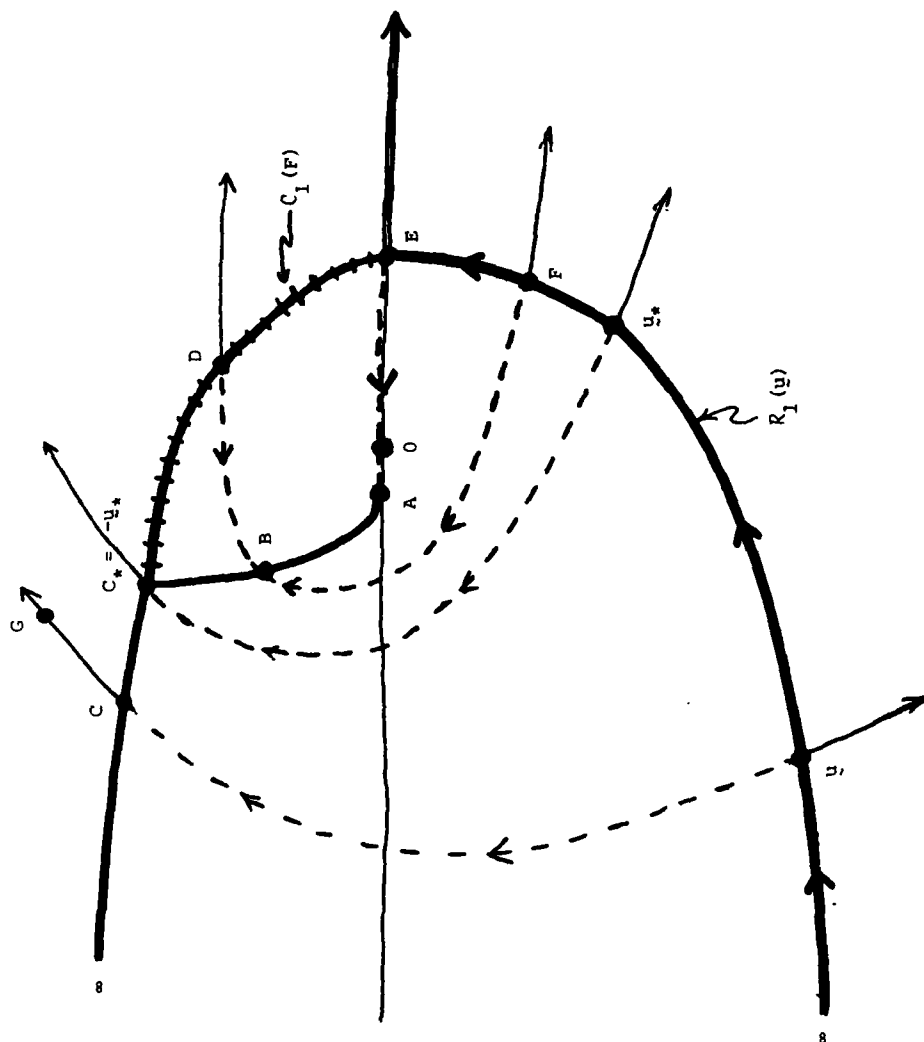


Figure 5

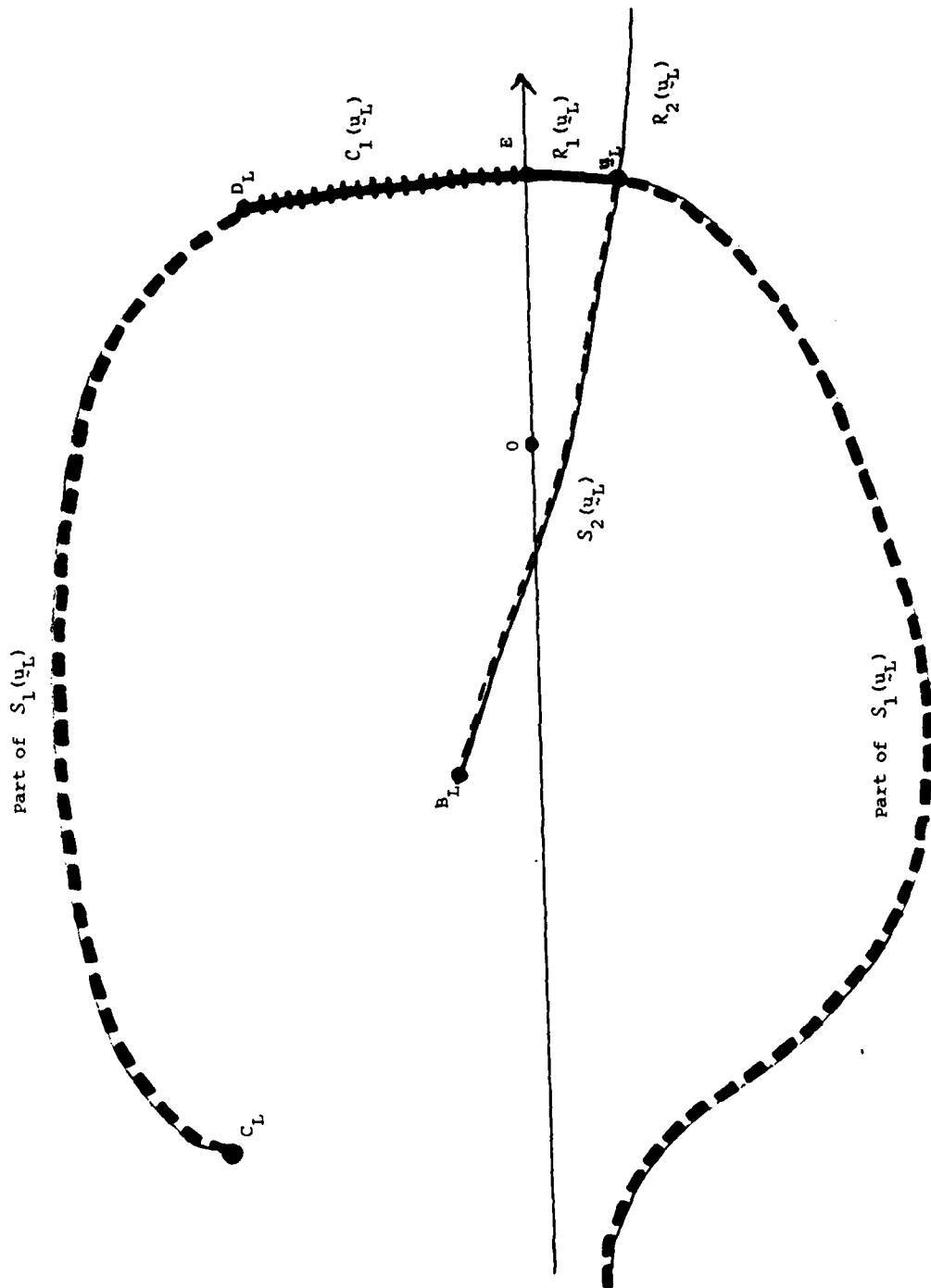


Figure 6A: The Wave Curves for $u_L \in A_1$

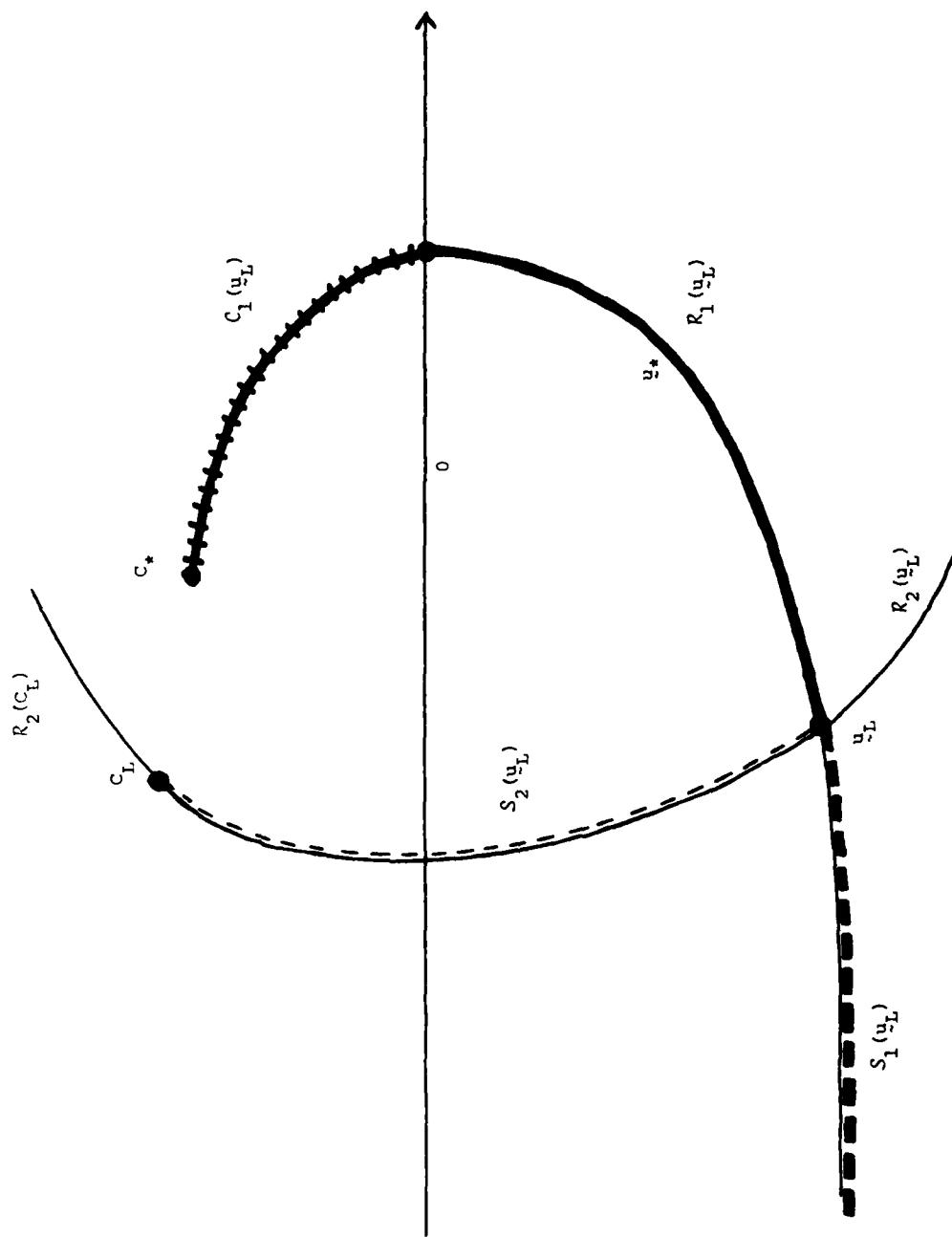


Figure 6B: The Wave Curves for $u_L \in \Lambda_2$

Figure 7A: Riemann problem solution for $\theta_L = 0$.

Figure 7B: Riemann problem solution for $\underline{u}_L \in A_1$.

Figure 7C: Riemann problem solution for $\theta_L = \theta_*$.

Figure 7D: Riemann problem solution for $\underline{u}_L \in A_2$.

Figure 7E: Riemann problem solution for $\theta_L = -\pi$.

Figure 7F: Riemann problem solution for $\underline{u}_L = \underline{0}$.

Figures 8A-D: Relationship between the axes and the lines $\lambda = 0$ for Regions I-IV.

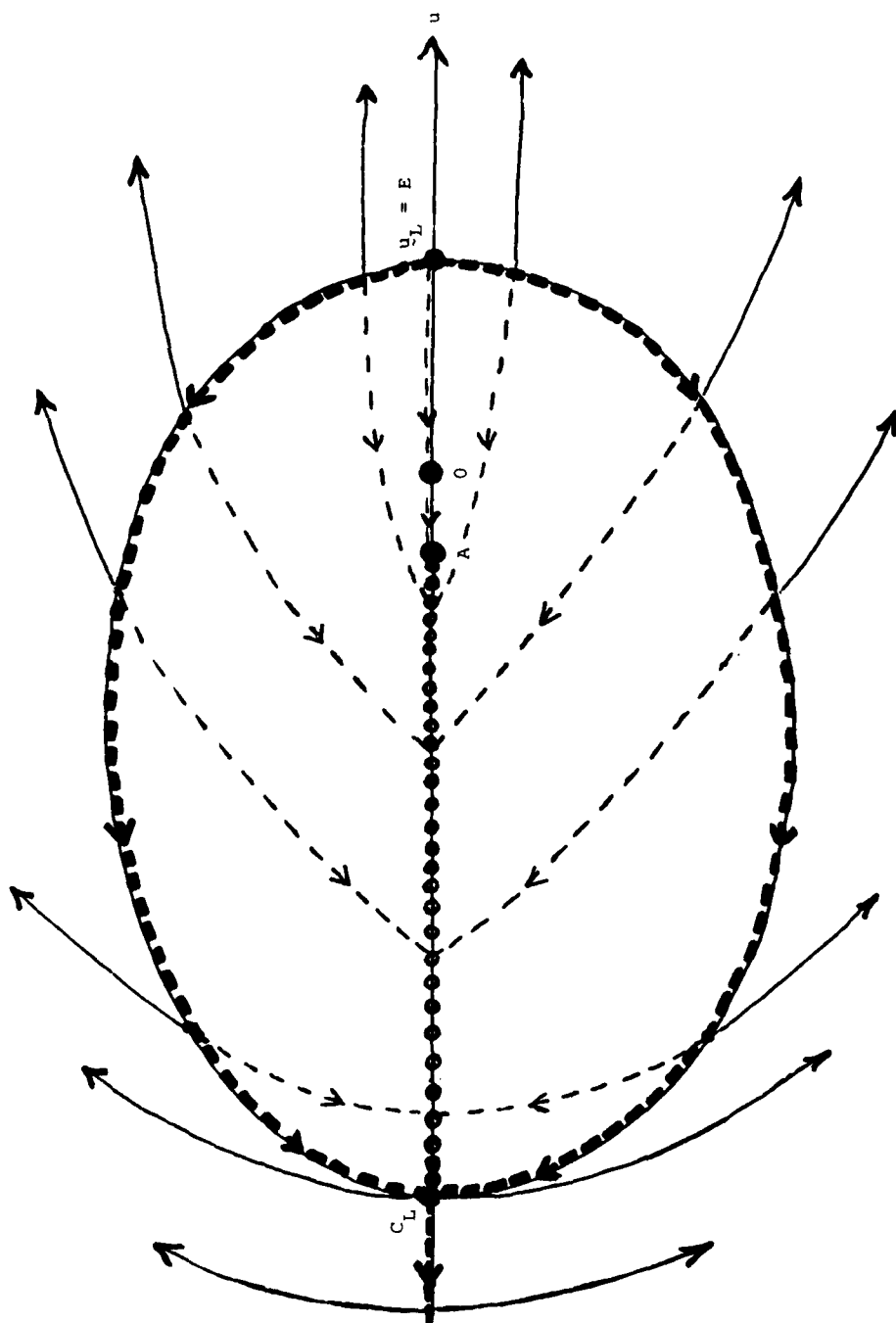
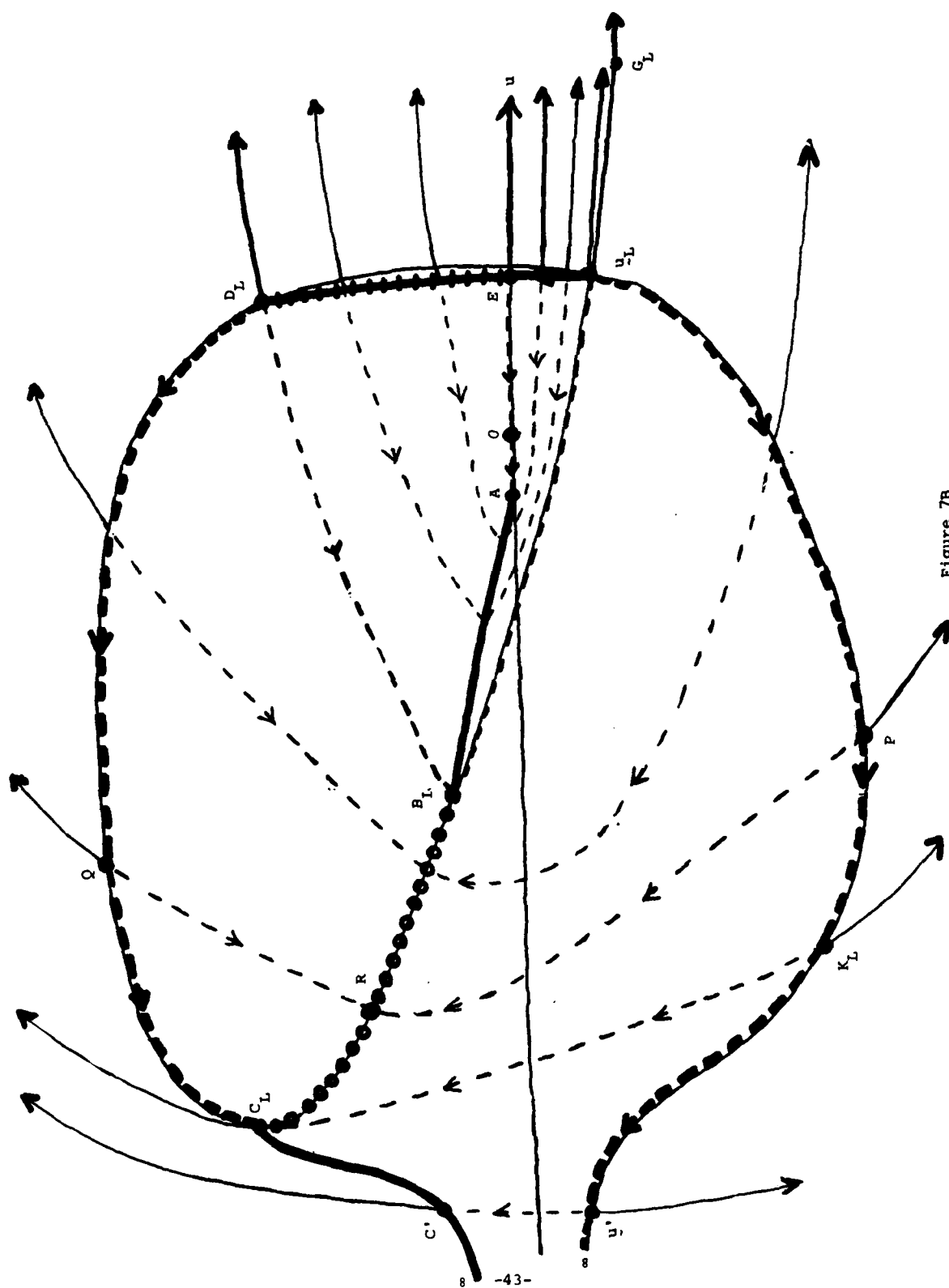


Figure 7A



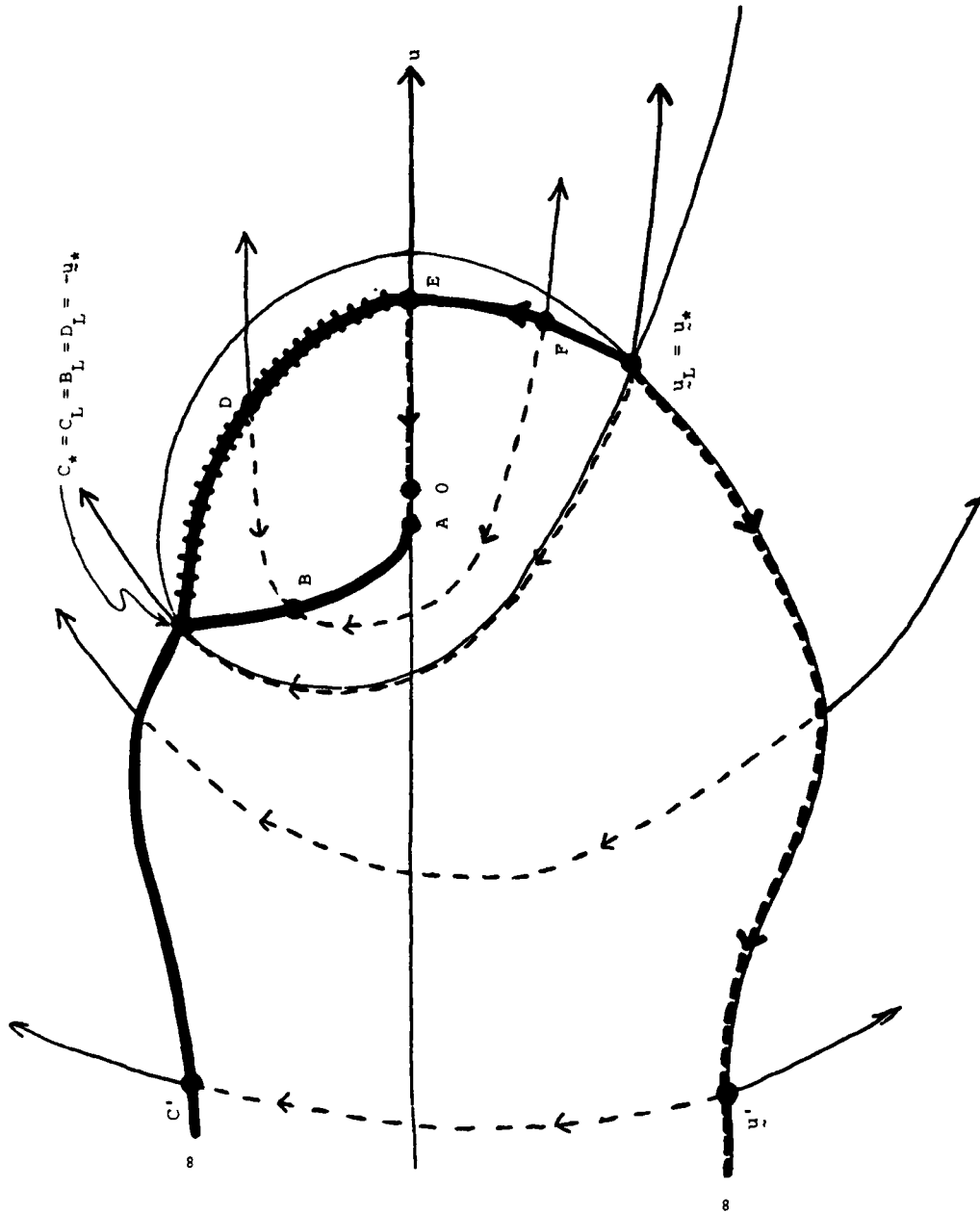


Figure 7C

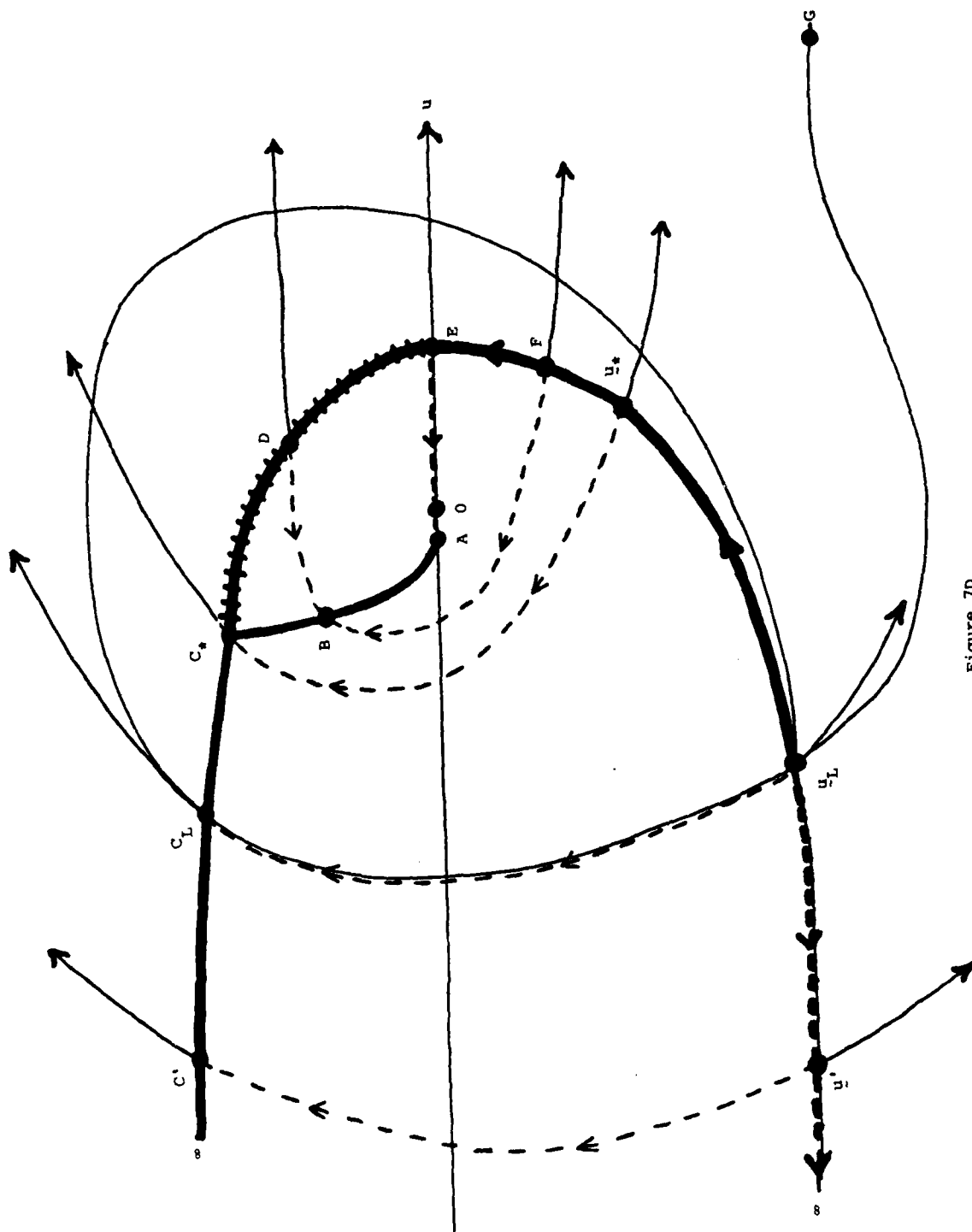


Figure 7D

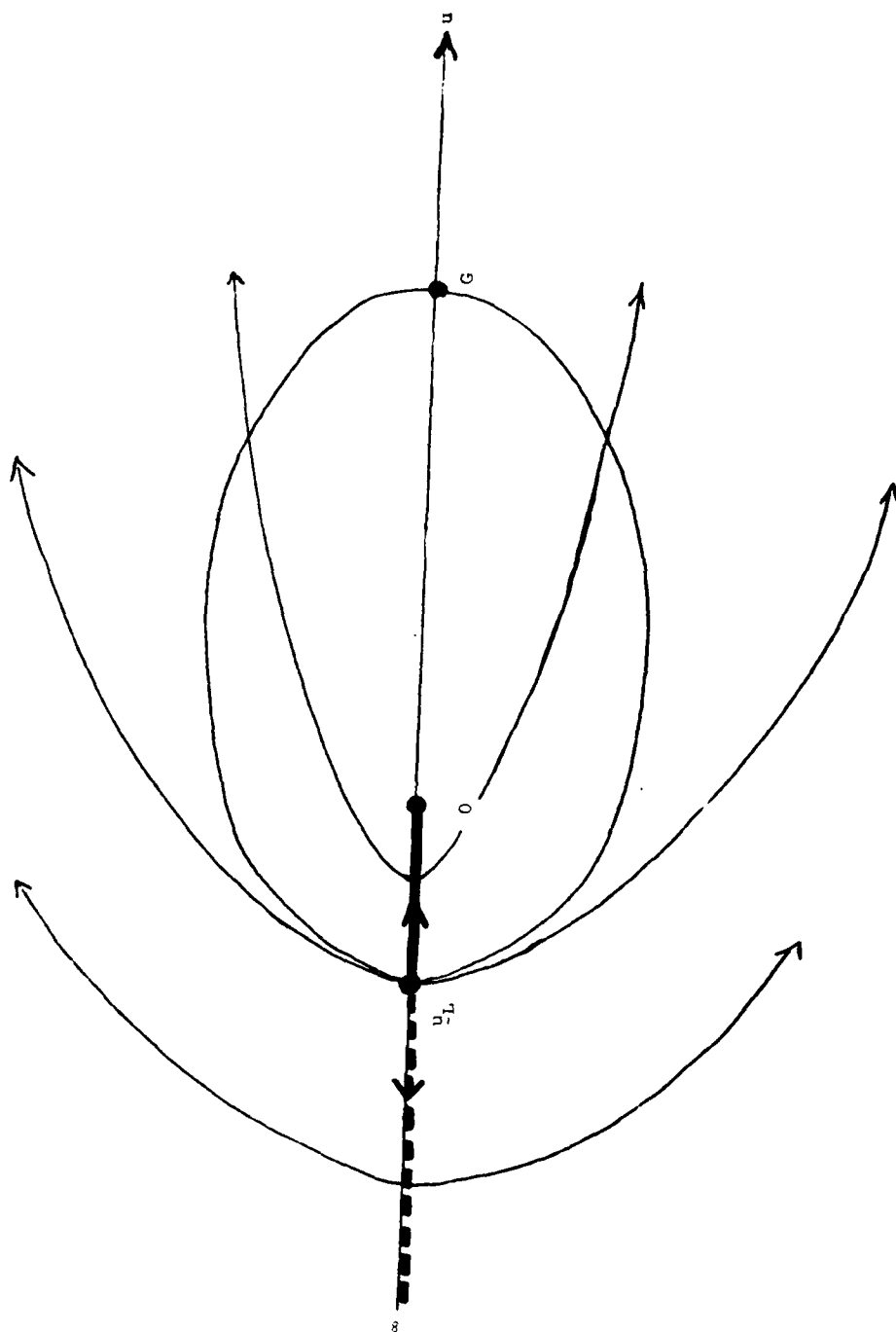


Figure 7E

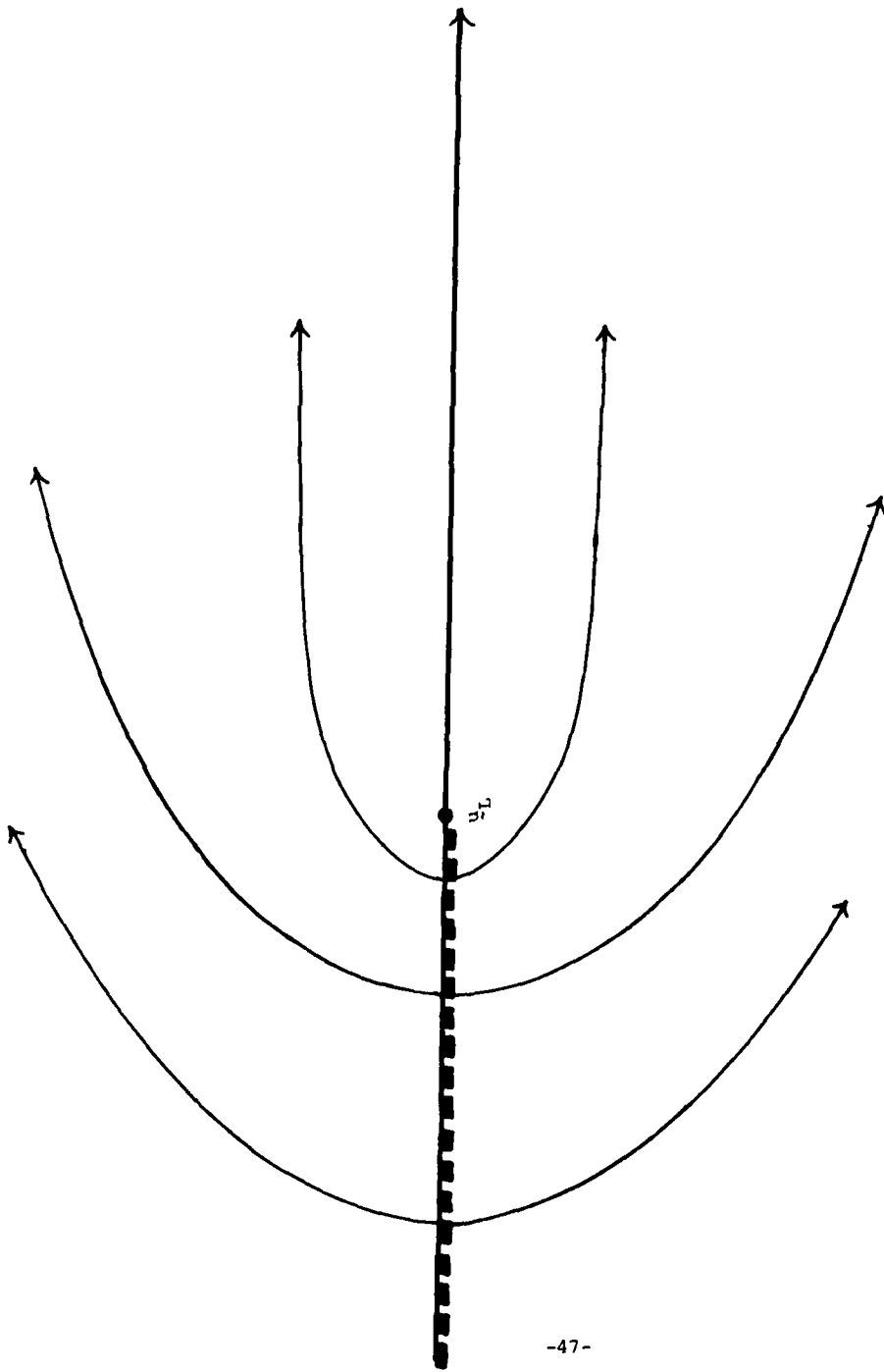
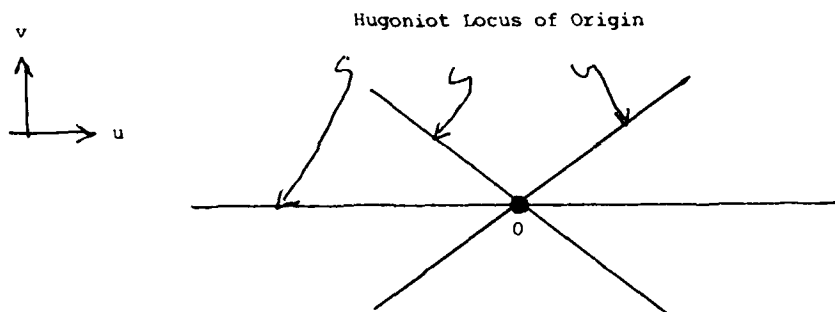
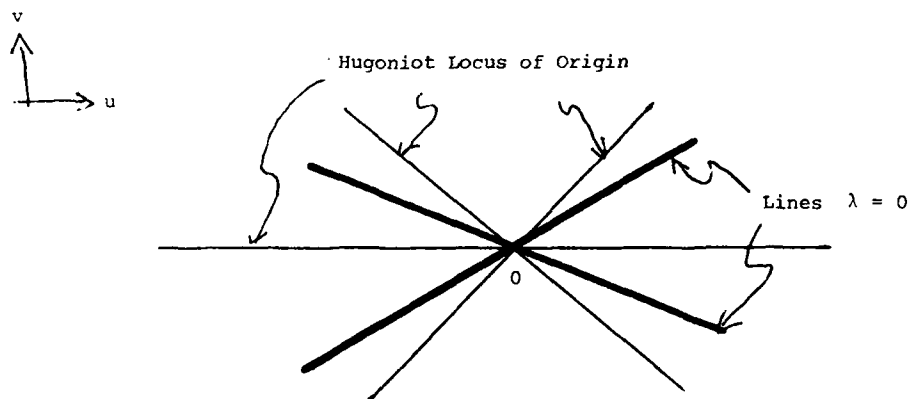


Figure 7F



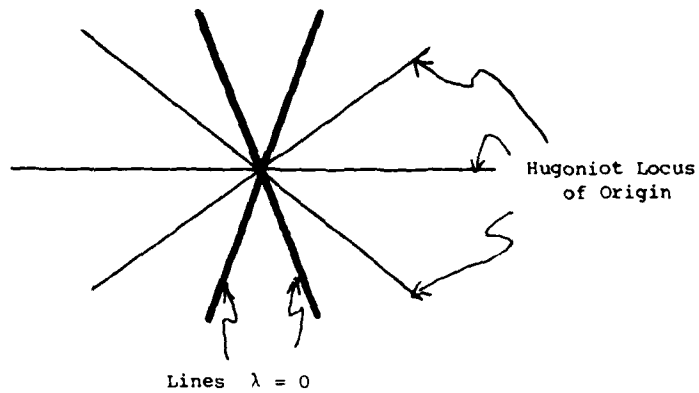
Region I: $\lambda = 0$ if and only if $u = 0$.

Figure 8A



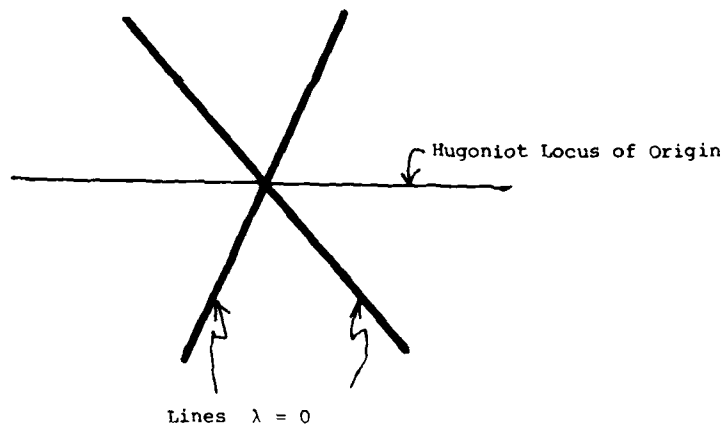
Region II

Figure 8B



Region III

Figure 8C



Region IV

Figure 8D

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) We are interested in classifying the solutions of Riemann problems for the 2×2 conservation laws which have homogeneous quadratic flux functions. Such flux functions approximate an arbitrary 2×2 system in a neighborhood of an isolated point where strict hyperbolicity fails. This problem was motivated by Marchesin and Paes-Leme who discovered such a singularity in a system of equations arising in oil reservoir simulation [15,17]. In [18], Schaeffer, Shearer, Marchesin and Paes-Leme solved the Riemann problem for this system in a neighborhood of the singular point. In [8], Isaacson and Temple outlined a		

20. ABSTRACT - cont'd.

program for classifying such singularities by means of locating normal forms for the equivalence classes of equations generated by linear changes in dependent variables. A 2-parameter family of such normal forms was found by Plohr. In the important work of Schaeffer and Shearer [17], a new normal form was found which reduced the classification of integral curves to a theorem of Darboux on the classification of umbilic points for homogeneous cubic equations [3]. The integral curves fall into four isomorphism classes, called Regions I-IV. In this paper we give the solution of the Riemann problem for the systems in Region IV which exhibit up-down symmetry. A presentation of the solutions of the corresponding systems in Regions II and III will follow.

Our analysis uses a numerical determination of the Hugoniot loci. Moreover, a new phenomenon occurs in Regions II-IV that does not occur in Region I: lines exist on which one of the eigenvalues has the value of the eigenvalue at the singular point. Bifurcations occur at these lines, and the dynamics of the lines as the parameters in the normal form are varied gives a geometric interpretation of the boundaries between Regions I-III. The program for classifying hyperbolic singular points in 2×2 systems of conservation laws is being carried out jointly by the authors named above.

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